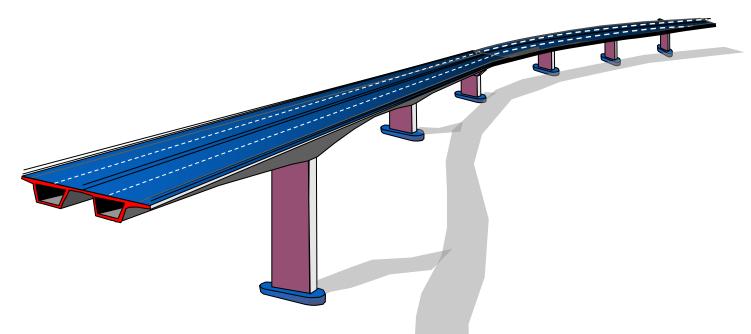




Construction Experience on Bridge/Elevated Structure



Athasit Sirisonthi, Ph.D

Advisor of Sub Committee of structural and bridge engineering
The Engineering Institute of Thailand Under H.M. The King's Patronage





- Introduction to Bridge Design and Construction
- Experience in Segmental Box-Girder Bridge/Elevated Structure





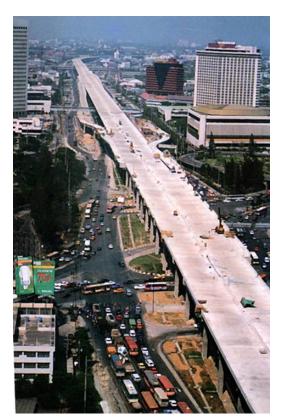
Introduction to Bridge Design and Construction





Introduction to Bridge Design and Construction

- Bridge/Elevated Structure Characteristic
- Bridge/Elevated Construction Concept



Don Maung Tollway @ Lad prao Intersection



SVB Airport Rail Link @ Soi Soon Vijai



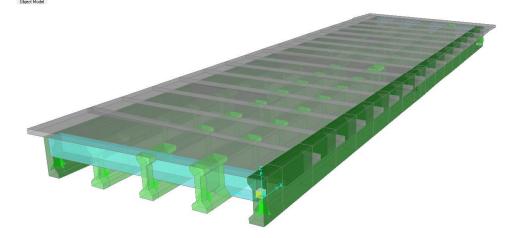


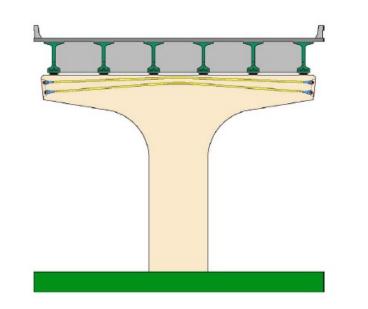


Bridge Superstructure: I-Girder with Deck slab

Bridge/Elevated Structures with I-Girder & Deck slab on Superstructure type, the old school design of bridge structure, this structure is use in many construction project in Thailand such as;

- Don Maung Tollway
- Expressway Stage 3: Section S1
- Elevated Frontage Road NBIA Project
- Overpassed Bridge by DOH, DOR
- Highway Interchange by DOH, DOR
- Etc.









Bridge Superstructure: I-Girder with Deck slab



Elevated Frontage Road NBIA Project – SV Joint Venture



The 3rd Stage Expressway S1: Contract 1 - Vichithan Construction Co., Ltd.

The method of erection I-Girder, which suitable for project "Mobile Crane" or "Launcher"





Bridge Superstructure: I-Girder with Deck slab



The 3rd Stage Expressway S1: Contract 1 - Vichitbhan Construction Co., Ltd.



The 3rd Stage Expressway S1: Contract 1 - Vichithan Construction Co., Ltd.

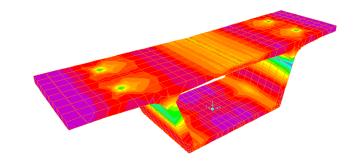
The construction of bridge deck slab can be separated into 2 type, one is composite deck slab with PC.Plank and the other one is Cast-In Placed slab



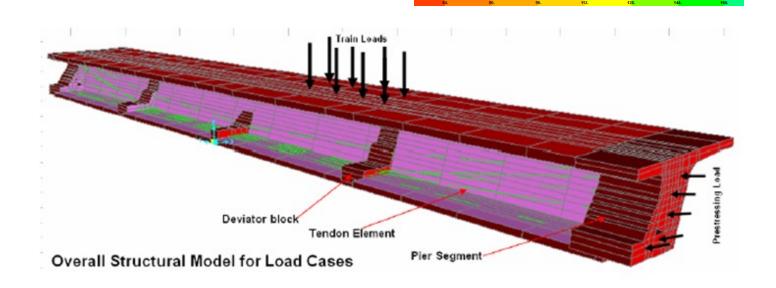


Bridge Superstructure: Box-Girder

Bridge/Elevated Structures with CIP. Box-Girder/PC. Box-Girder on Superstructure type, the modern design of bridge structure, this structure is use in many construction project in Thailand such as;



- Expressway Stage 2
- BTS Elevated Structure
- Airport Rail Link
- MRT Purple Line/Blue Line
- Sri Rat Expressway
- Etc.







Bridge Superstructure: Cast-In Placed Box-Girder







Industrial Ring Road - STECON

The method of construction Box Girder is separated into 2 type, one is by using "Movable Scaffolding System" and the other one is "Conventional Shoring"

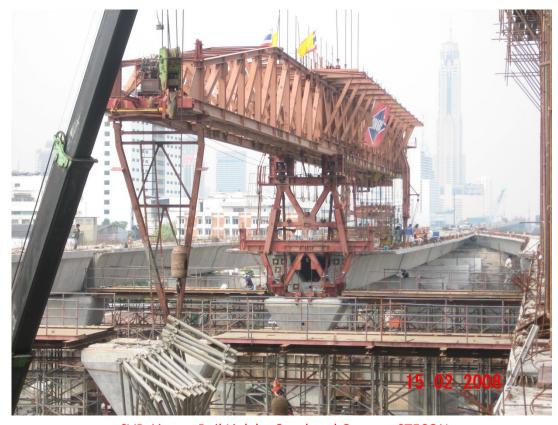




Bridge Superstructure: PC. Segmental Box-Girder



SVB Airport Rail Link by Underslung Gantry – STECON & VSL



SVB Airport Rail Link by Overhead Gantry - STECON

The Equipment that use to erection PC. Segmental Box Girder call "Launcher" which can separated into 2 type, one is "USG: Underslung Gantry" and the other one is "OHG: Over Head Gantry"





Experience in Box-Girder Bridge/Elevated Structure





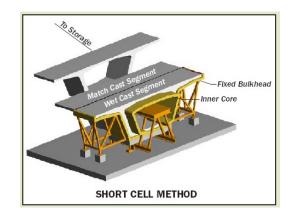
Experience in Box-Girder Bridge/Elevated Structure

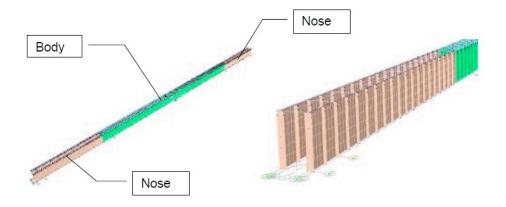






Construction of Precast Segmental Box-Girder Span by Span Erection





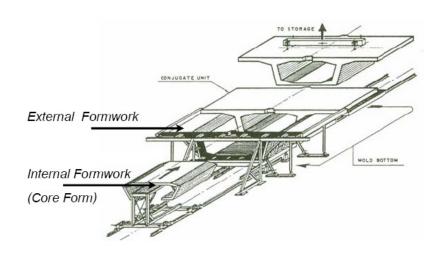


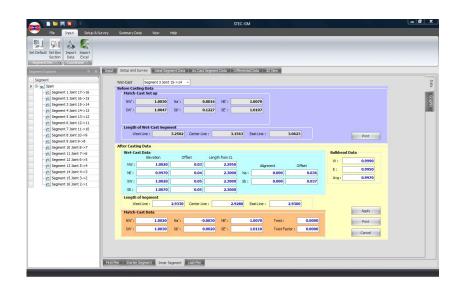


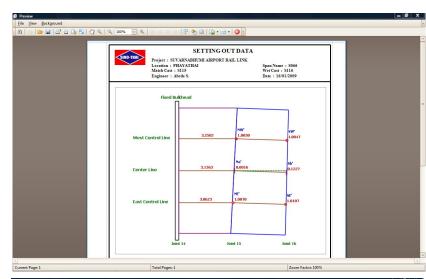
Precast Segmental Box-Girder: Segment Production

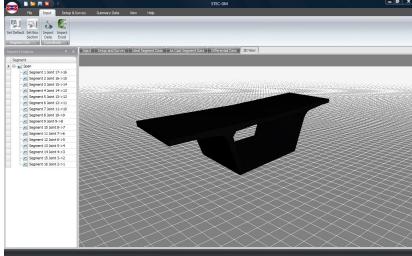
The segments for erection viaduct has produced by Short-Line Casting Method that need the method of Calculation to control alignment and profile of bridge structure call "Geometry Control"

STECON has developed "Geometry Control Software" for use to control our production of precast segmental box-girder erection, STEC-GM can generate Setting Out data for match cast segment and recheck As-casted Data for erection and control error of production in limitation of specification and practice code. It can show casted span in 3 Dimensional and show N,E,Z of As-Casted span compare to Span Layout





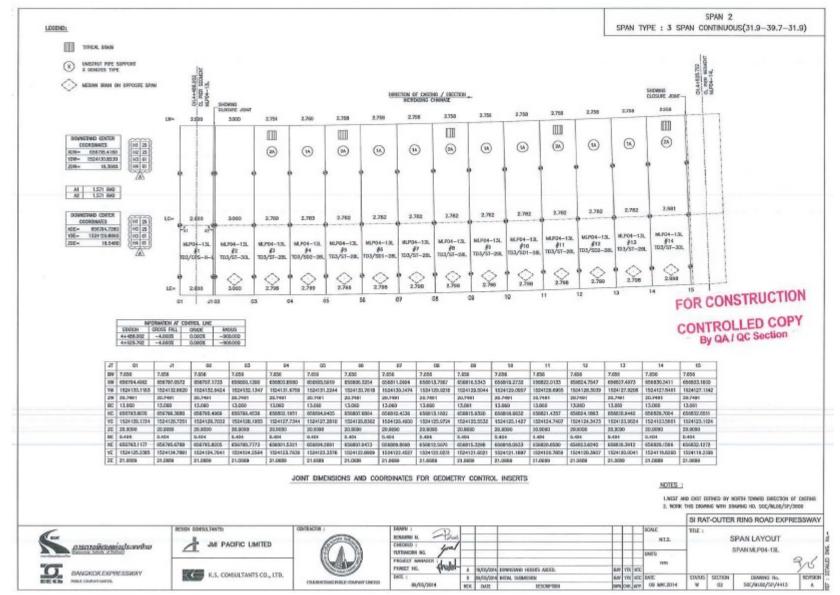








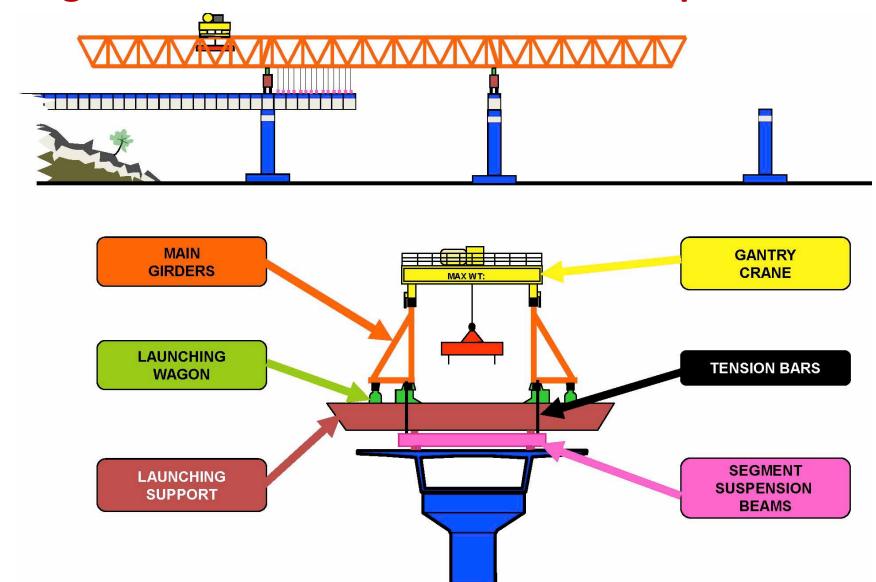
Precast Segmental Box-Girder: Segment Production







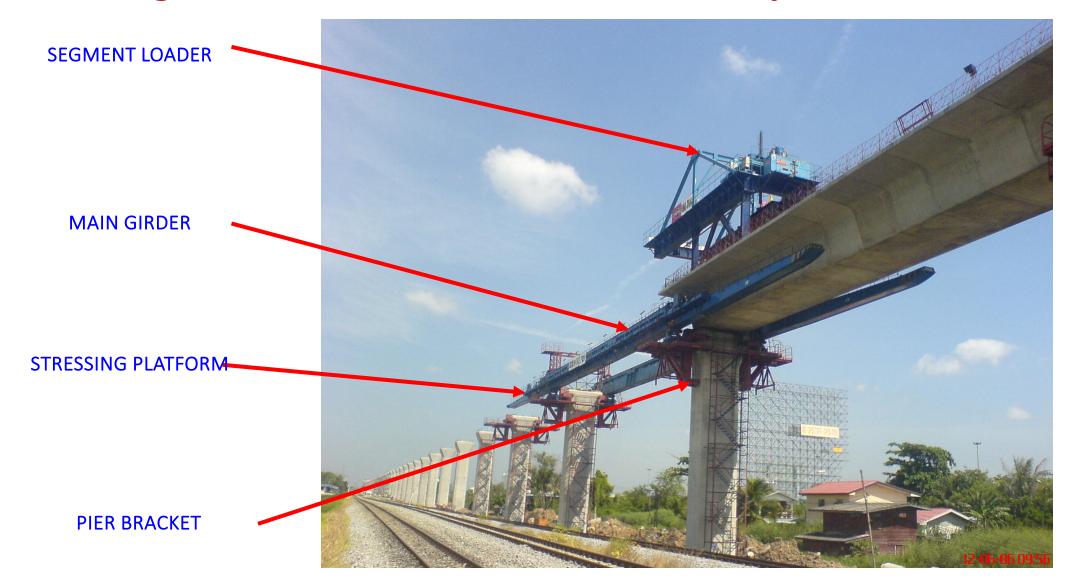
Precast Segmental Box-Girder: Launcher Component







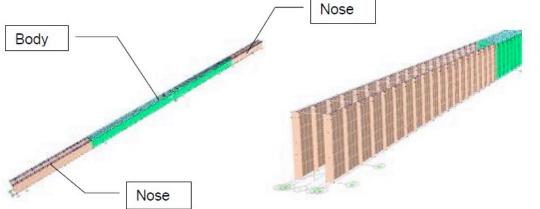
Precast Segmental Box-Girder: Launcher Component













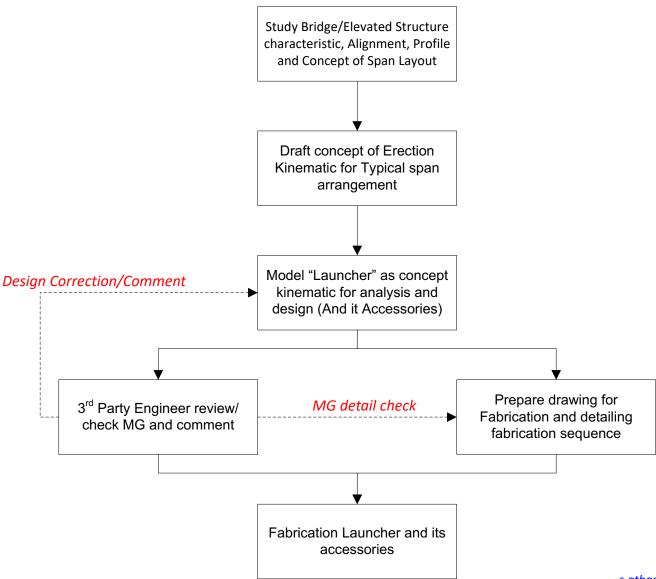


Design process workflow of "Launcher" for erection works in every project of STECON as shown.

Structural analysis, design and detail of fabrication drawing by STECON engineer will be done and send to 3rd Party design firm to check before start fabrication.

The report of 3rd Party check will be considering into in depth of structural engineering such as review analysis by FEM: Finite Element Model, Local failure analysis, Stability analysis, Dynamic analysis of Free vibration response due to Launcher self weight, Joint connection capacity check, deflection check and Safety Factor check at each stage.

After report review and comment, Launcher Fabrication will be start and witness by Engineering Team & Launching Operation







DESIGN CRITERIA:

1. MATERIAL PROPERTIES:

Structural Steel: Grade A572Gr50 Yield Strength 345 MPa Ultimate Strength 450 MPa Modulus of Elasticity 200,000 MPa Yield Strength 400 MPa Grade \$450 Ultimate Strength 650 MPa Modulus of Elasticity 200,000 MPa Stressing Bar; Grade 1050/1200 Yield Strenath 1.050 MPa Ultimate Strength 1.200 MPa Modulus of Elasticity 205,000 MPa Ultimate Tensile Strength Weld Electrode: Grade E70 480 MPa

2. DESIGN REFERENCE:

- 1. American Institute of Steel Construction, Allowable Stress Design, 9th Edition
- 2. Engineering Institute of Thailand (E.I.T. Standard)
- 3. Steel Table for Contractor and Engineer (Tee Group of Engineers)

MOVING STEP POSITION FOR CHECK STRESS:

Step-1 for Erection Gantry Installation

Step-2 for Load Segment (By Unimoc)

Step-3 for Lifting & Segment Installation

Step-4 for Lowering Segment

Step-5 for Movement of Erection Gantry (Launching to next Step 1)

Step-6 for Movement of Erection Gantry (Launching to next Step 2)

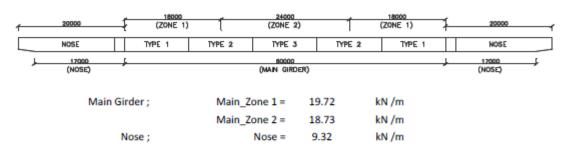
Step-7 for Movement of Erection Gantry (Launching to next Step 3)

Step-8 for Setup Bracket Type 3 and Remove Bracket Type 1 (Launching to next Step 4)

Step-9 for Remove Bracket Type 1 to Setup on Next Pier (Launching to next Step 5)

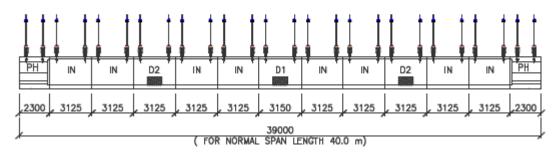
Step-10 for Cantilever to next span & Installation of Bracket on next span

Load Case 1, LC1: Selfweight of Gantry



Load Case 2 , LC2 : Segment weight Type DH21

(Max.of Segment weight in Purple Line Project)



Example of Calculation detail

- Design Criteria
- Load Case calculation





Sections Properties - Erection Gantry_Main Member

NO.	h	b	Α	dy	lx-x	<u>D</u>	A* <u>D</u> 2
	(cm)	(cm)	(cm²)	(cm)	(cm ⁴)	(cm , ref. N.A.)	
Member 1	1.40	50.00	70.00	329.30	11.43	162.63	1,851,294.79
Member 2	22.20	1.80	39.96	317.50	1,641.16	150.83	909,023.88
Member 3	1.40	50.00	70.00	305.70	11.43	139.03	1,352,967.18
Member 4	2.00	180.00	360.00	304.00	120.00	137.33	6,788,990.06
Member 5	100.00	2.40	240.00	253.00	200,000.00	86.33	1,788,503.99
Member 6	124.50	2.40	298.80	90.75	385,956.23	75.92	1,722,439.37
Member 7	2.00	130.00	260.00	27.50	86.67	139.17	5,036,077.41
Member 8	1.40	50.00	70.00	25.80	11.43	140.87	1,389,192.82
Member 9	22.20	1.80	39.96	14.00	1,641.16	152.67	931,447.17
Member 10	1.40	50.00	70.00	2.20	11.43	164.47	1,893,629.21
Member 11	1.50	44.00	66.00	0.75	12.38	165.92	1,817,041.00
Member 12							

Total;	H =	330.00	cm	C.G.(Y) =	166.67	cm
	Ag =	1584.7200	cm ²	Ic.g. =	0.2607	m ⁴
	r =	1.6451	m			
	Ct =	1.6333	m	St =	0.1596	m³
	Cb =	1.6667	m	Sb =	0.1564	m ³

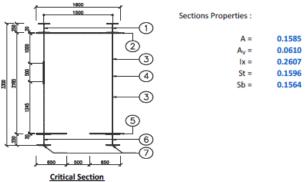
W (Ton/m) W+35%(Ton/m) 1.24 1.68

MARK NO. NO. 1 = H-250x250x9x14, 72.4 kg/m (Top Member) NO. 2 = PL 20 mm Thk. (Top Plate) NO. 3 = PL 12 mm Thk. (Web Plate) NO. 4 = Hole Dia. 500 mm NO. 5 = PL 20 mm Thk. (Bottom Plate) NO. 6 = H-250x250x9x14, 72.4 kg/m (Bottom Member) NO. 7 = PL 15 mm Thk. (Lower Plate) * All Dimensions are in Millimeters

Example of Calculation detail

- Section properties
- Joint Connection

Design Joint Connection:



Moment capacity;

Use min value of M to control the design

Allowable , Fb =	207.00	Mpa
Top fiber , Mt =	33.04	MN-m
Bottom fiber , Mb =	32.37	MN-m
Thus, Design Moment ca	pacity of Joint =	34.00

Shear capacity

Use A_V of Section to control the design

Allowable , Fv =	138.00	Mpa	
Area, A =	0.06	m ²	
Shear, V =	8.42	MN	
Thus, Design Shear ca	pacity of Join	t =	9.00

Moment design;

Use HSTR Bar Tensile Strength Dia. 75 mm

ar Tensile Strength Dia. 75 mm			
Meterial Properties:	Fy =	1,050.00	Mpa
	Fu =	1,200.00	Mpa
	E =	205,000.00	Mpa
	Elongation =	10.00	%
For Dia 75 mm :	100% Fy =	4,561.00	kN
	70% Fu =	3,649.00	kN (Working Load)

Prestressing Force (10% of Working Load) = 364.90 kN Thus , Remain capacity = 3.28 kN / Bar

Trial Moment arm , R = 2.40 m

Force , T = 14.17 MN

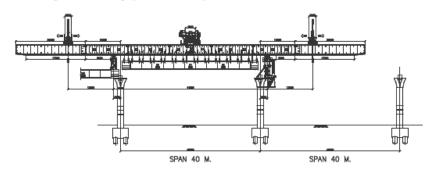
No. of Stress Bar = 4.31 Piec

Use Stress Bar , No. = 5.00 Piece s.athasit@gmail.com





Check Stage-3: Launching Span 40.0 m to Span 40.0 m



Stage-3: Lifting & Segment Installation
COMB3: LC1 + (1.3xLC2) + LC4 + LC5 + LC6 + (1.3xLC7) + LC9

Reactions - kN, kN m







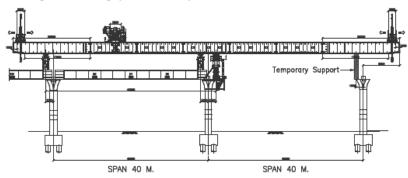
Summary: Analysis Results COMB3 (Span 40.0 m to Span 40.0 m)

Reactio	ın (kN)	Shear (kN) Moment (kN			
R1	R2	V-	V+	M-	M+
3,333.38	3,333.38	2,862.32	2,862.32	5,567.94	28,146.00

Example of Calculation detail

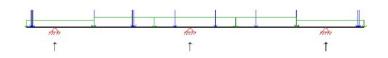
- Erection stage
- Launching stage

Check Stage-8: Launching Span 40.0 m to Span 40.0 m



Stage-8 : Setup Bracket Type 3 and Remove Bracket Type 1 (Launching to next Step 4) COMB8 : LC1 + LC4 + LC5 + LC6 + LC9

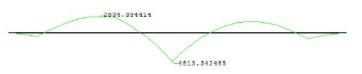
Reactions - kN, kN m



Shear - kN



Moment - kN m



Summary: Analysis Results_COMB8 (Span 40.0 m to Span 40.0 m)

	Reaction (kN)		Shear	(kN)	Moment	(kN - m)
R1	R2	R3	V-	V+	M-	M+
423.79	1,200.41	442.42	642.68	557.74	4,813.34	2,834.39

Max.Deflection: $\Delta_{max} = 8.14$ r

Max.Deflection: $\Delta_{max.} = 103.36$ mm





Summary: Analysis Results

Launching Span 40.0 m to Span 40.0 m:

Store		Reaction (kN)		Shear	(kN)	Moment	Moment (kN - m)	
Stage	R1	R2	R3	V-	V+	M-	M+	
Stage - 01	1,091.81	1,091.81	-	620.75	620.75	5,567.94	1,762.86	
Stage - 03	3,333.38	3,333.38	-	2,862.32	2,862.32	5,567.94	28,146.00	
Stage - 04	3,333.38	3,333.38	-	2,887.28	2,887.28	5,242.94	15,687.04	
Stage - 07	482.28	1,241.12	343.23	684.11	557.01	5,185.47	4,018.61	
Stage - 08	423.79	1,200.41	442.42	642.68	557.74	4,813.34	2,834.39	
Stage - 09	388.08	1,082.73	595.82	555.89	526.84	4,159.33	2,197.15	
Stage - 10	390.26	1,070.61	670.75	553.70	516.90	4,071.95	2,234.28	

Launching Span 35.0 m to Span 40.0 m:

Stage		Reaction (kN))	Shear	(kN)	Moment (kN-m)		
Stage	R1	R1 R2		V-	V+	M-	M+	
Stage - 01	1,091.81	1,091.81	-	568.53	568.53	6,748.37	0.01	
Stage - 03	3,333.38	3,333.38	-	2,810.20	2,810.20	6,748.37	23,151.60	
Stage - 04	3,333.38	3,333.38	-	2,835.06	2,835.06	6,423.37	13,020.02	
Stage - 07	570.61	1,125.96	370.05	595.78	530.18	4,214.43	3,181.81	
Stage - 08	506.12	1,099.10	461.39	560.34	538.76	4,050.60	2,284.21	
Stage - 09	462.57	991.64	612.41	481.39	510.25	3,492.34	2,226.55	
Stage - 10	465.26	978.85	687.51	478.70	500.15	3,398.24	2,112.25	

Summary Maximum:

Reaction (R) = 3,333.38 kN

Shear (V-) = 2,887.28 kN

Shear (V+) = 2,887.28 kN

Moment (M-) = 6,748.37 kN - m

Moment (M+) = 28,146.00 kN - m

Max.Deflection (Δ_{max.}) = 103.36 mm

Example of Calculation detail

- Summary analysis result
- Design of MG

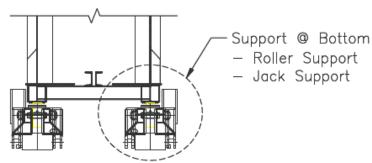
e Girder Design :										
Design Parameters				Section Prop						
Yield Stress of Steel (A572Gr50)	Fy	= 345.00	MPa	Section Name						
Modulus Elasticity of Steel	E	= 200,000.00	MPa	Width of Sec			bf	-	1,800.00	mm.
Max. Actual Member Length Max. Unbraced Length of Beam	L Low	= 60,000.00 = 1,000.00	mm. mm.	Depth of Sec Flange Thicks			d t _f	-	3,300.00	mm. mm.
Bending Coefficient	C	= 1.00	men.	Web Thickne			t _w		12.00	mm.
Yield Stress of Electrorode, Grade E70	Fine	= 480.00	MPa	Clear Distance			h	-	2.760.00	mm.
The stress of Energy Group, Group Ero	- 870	- 100.00		Gross Section			A,		158,472,00	mm.2
				Moment of I			I.	_	2.607E+11	mm.4
				Section Mod			S,		156413353	mm.3
				Radius of Gyr		X-Axis	r _x	-	1,645.09	mm.
				Radius of Gyr	ration of	Section	rr		1,645.09	mm.
				Area of Flang	e		A,		36,000.00	mm.2
				Area of Web			A.		66,240.00	mm.2
Designed Force Considered in the Design	1									
Max. Bending Moment	М	= 28,146,000.00	kN-mm.							
Max. Shear Force	V	= 2,887.28	kN							
Max. Reaction Force at Support	R	= 3,333.38	kN							
Max. Vertical Deflection	Δv	= 103.36	mm.							
Determination of Design Criteria and Sec										
		138.68		c h/t _w	-	230.00			R DESIGN	
	38(E/F _p) ^{0.8}			c b _i /2t _i	-	45.00	NON-CO	MPA	ст	
		°= 19242.47	mm.							
		= 4363.64	mm.							
Thus; Max. Unbraced Length	Le	= 4363.64	mm.	» L _b	-	1000	CASE I			
Computation of Allowable Bending Stress	rı E.									
Case I: L _b ≤ L _c For Compact Section			MPa							
For Non-Compact Section			MPa							
To Non-Compact Section	, p - 0.000 y	- 220000								
Case II: L _b > L _c For All Section	L/r_{τ}									
(3.517EC ₄ /F ₄) ^{2.60}		= 45.15	mm.	c L/rr						
(17.586EC _b /F _y) ^{0.80}		= 100.97	mm.	c L/rr						
● IF L/r _T ≤ L _{min}	0.60F		MPa	4.1						
• IF L _{min} < L/r _Y < L _{max} (2/3-F _y (L/r _Y) ² /52				0.60F _v	-	207.00	MPa			
	Ch/(L/r _t) ²		MPa	0.60F	-	207.00	MPa			
Thus; Allowable Bending Stress		= 120000.00	MPa							
Allowable Bending Moment	M=FaS,	= 1.87696E+13	kN-mm.	> M	-	2.81E+07	kN-mm.		PASS	
Computation of Reduced Allowable Bend	9									
0.6F _{yw} /F _b	CT R	= 0.00 = 0.77		< 1.00 < 1.00		0.00				
(12+(A _a /A _a)(3α-α ^b))/(12+2(A _a /A _a)) (1-(0.0005A _a /A _a (h/t _a -5.76(0.6.E/F _a) ^{2.b}))	R _s Rpg	= 0.77		< 1.00 < 1.00		0.77				
Reduced Allowable Bending Stress		= 125.84	MPa	2.00	_	0.75				
Reduced Allowable Bending Moment			kN-mm.	> M	-	2.81E+07	kN-mm.		PASS	
Computation of Allowable Shear Stress; F	Pv									
Web Sienderness Limitation :										
Transverse Stiffener Requirement	h/t	= 230.00		h/t w	<	260		^	IOT REQUIRED	,
Max. Intermediate Web Stiff. Spacing	-	= 8280 = 3527	mm. mm.							
Intermediate Stiffener Spacing	a and the control of	= 500	mm.							
	a/h	= 0.18		< 1			ONTROLLE	מ שו	H TENSION FIEL	D ACTION
		= 282.67								
	4(E/F_)***	- 202.07								
● IF a/h≤1.50 11.7 ● IF a/h> 1.50 0.48E/(F _y		= 202.07								
● IF a/h≤1.50 11.7	(F _V +F _r)) ^{0.5} h/t w			h/t "	<	260			PASS	
● IF a/h≤1.50 11.7 ● IF a/h> 1.50 0.48E/(F _y	$(F_y+F_r))^{0.5}$			h/t "	<	260			PASS	
● IF a/h≤1.50 11.7 ● IF a/h>1.50 0.48E/(F _y (SE/F _y) ^{0.5} = 53.84 <	(F _y +F _r)) ^{0.5} h/t _w	= - = 230.00		h/t "	<	260			PASS	
• IF $a/h \le 1.50$ 11.7 • IF $a/h \ge 1.50$ 0.48E/ $(F_y)^{a/h} = 53.84$ • IF $a/h < 1$ 4.00 + $5.34/(a/h)^2$ • IF $a/h > 1$ 5.34 + 4.00/ $(a/h)^2$ • 1.55x $e/(h/t_w)^2$	(F _y +F _r)) ^{0.5} h/t _w k, k, c,	= - = 230.00 = 166.711936 = -		h/t "	<	260			PASS	
■ IF $a/h \le 1.50$ 11.7. ■ IF $a/h > 1.50$ 0.48E/[F _j ■ IF $a/h > 1.50$ 0.48E/[F _j ■ IF $a/h < 1$ 4.00 + 5.34/(a/h) ² ■ IF $a/h > 1$ 5.34 + 4.00/(a/h) ² ■ 1.15%, $E/(h/t_{-})^2 F_0$ ■ 1.12(E/F_j) = E/F_j) = E/F_j =	(F _v +F _r)) ^{0.5} h/t w k v k v v v C v	= . = 230.00 = 166.711936 = . = . = 1.51		h/t "	<	260			PASS	
• IF $a/h \le 1.50$ 11.7. • IF $a/h \ge 1.50$ 0.48£/F _F • IF $a/h \ge 1.50$ 0.48£/F _F • IF $a/h \ge 1.50$ 0.48£/F _F • IF $a/h \ge 1.50$ 4.40 $a/h \ge 1.50$ 4.50 4.50 4.50 4.50 4.50 4.50 4.50 4.50 4.50 4.50 4.50 4.50 4.50 4.50 4.50 4.50 4.50	(F _y +F _t)) ^{0.5} h/t w k v k v c v c v c v f C v so f F v	= 230.00 = 166.711936 = - = 1.51 = 128.23	MPa		<				PASS	
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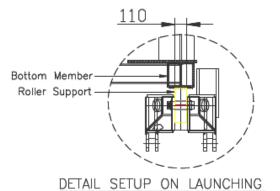


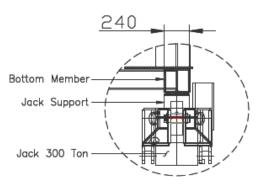


Check Bottom Member form Concentrated Load :

Point Load :	P =	3,333.38	kg	(Max.Rea	action)			
Material Properties :	Fy = E =	3,250.00 2,040,000.00	ksc ksc					
Section Properties :	d = b = tf = tw = r = k = N =	25.00 25.00 1.00 1.00 1.80 3.30	cm cm cm cm cm cm	ise min. = k	x)			
Check Web Yielding; A) Load on mid s	pan (> d/2) f _{Bearing} =	192.68	ksc	<	2,145.00 (0.66Fy)	ksc	O.K.	Example of Calculation detail
B) On support	f _{Bearing} =	323.63	ksc	<	2,145.00 (0.66Fy)	ksc	O.K.	Check concentrate Load
Check Web Crippling; A) Load on mid s	pan (> d/2) P max. =	45,467.61	kg	>	3,333.38	kg	O.K.	 Design support
B) On support (<	d/2) P max. =	22,733.81	kg	>	3,333.38	kg	O.K.	
Check Sidesway Web Buckling ;	L = dc = v)/(L/bf) =	100.00 18.40 4.60	cm cm					
A) When (dc/tw	P max. =	762,523.41	kg	>	3,333.38	kg	O.K.	
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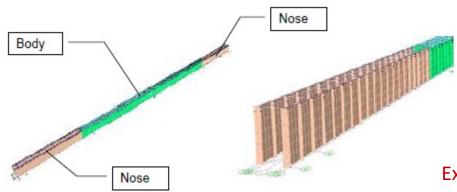












Example of 3rd Party check

- FEM analysis check
- Dynamic response

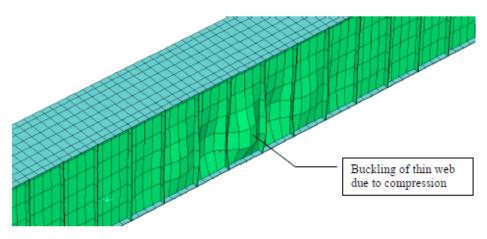


Figure 3.10 Lowest buckling mode: Local bend buckling of gantry web

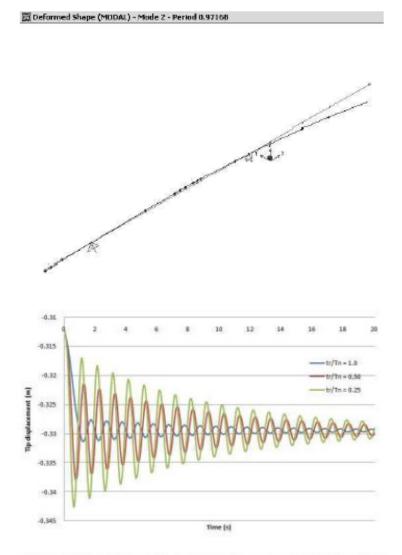


Figure 3.8 Time history of tip displacement for various t, /T, (Stage IV.1)





Precast Segmental Box-Girder: Launcher Accessories



RS - Roller Support



PB - Pier Bracket



LCB - Lower Cross Beam



WF - Winch Frame



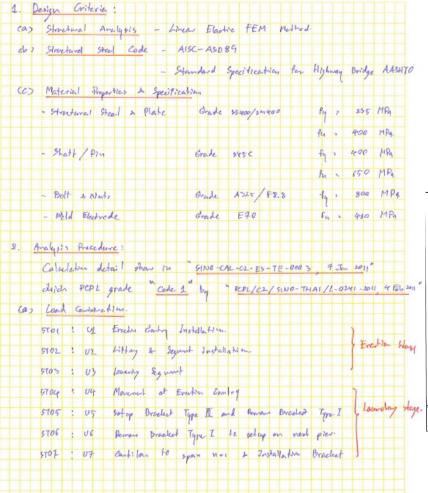
LSU - Lowering Span Unit





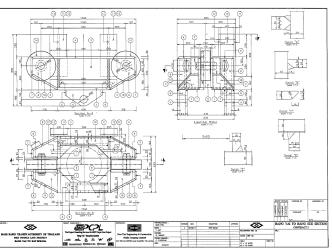
Precast Segmental Box-Girder: Accessories design



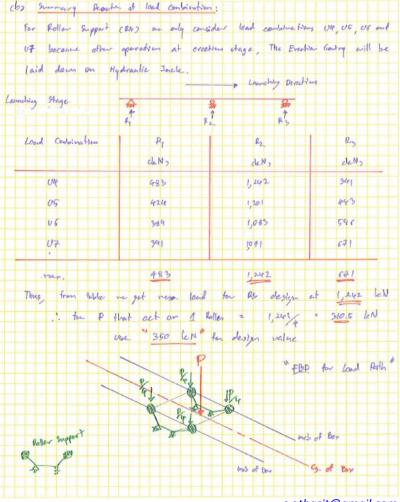


RS – Roller Support Calculation

- Design Criteria
- STR Model and Load Case











Precast Segmental Box-Girder: Accessories design

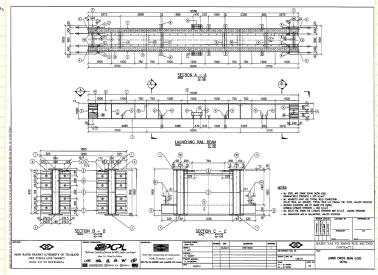


do Load Combination:

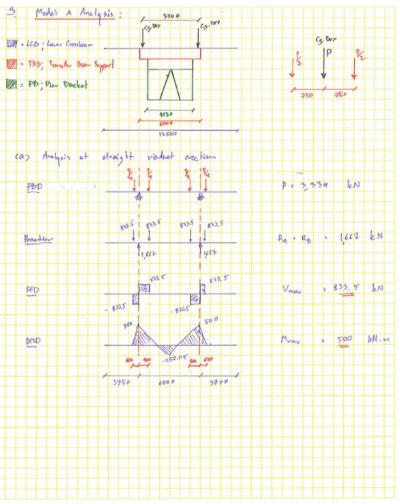
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LCB – Lower Cross Beam

- Load Case and Combination
- STR Model and Analysis











Precast Segmental Box-Girder: Launcher Documents

Before Launcher Operation ESS will finished all Engineering Document as follows;

- Design Calculation & Drawing
- Assembly Method
- Launching Kinematic
- Construction stage check of substructure
- Load transfer calculation
- Launcher Method and Load Test Result

All document will be submit to CSC, STECON QA/QC team, Launching Operation Team to do as design procedure from ESS Team

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Precast Segmental Box-Girder: Launcher Documents



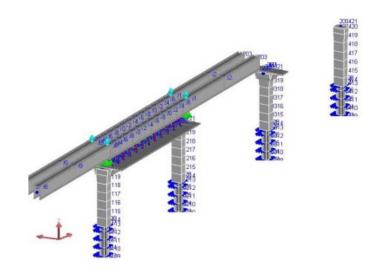
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MRTA BLUE LINE EXTENSION PROJECT CONTRACT 4: ELEVATED CIVIL WORK

CALCULATION OF LOAD TRANSFER BY OVERHEAD GANTRY

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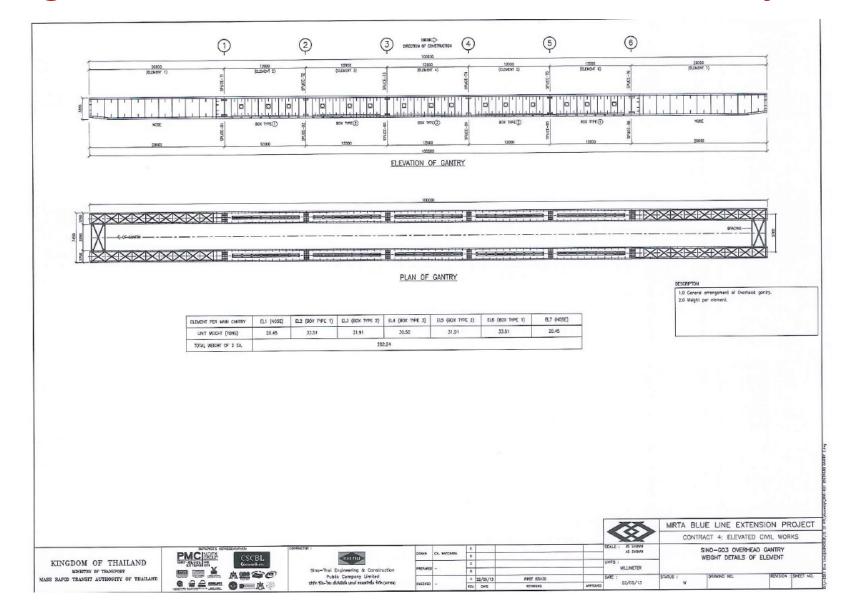
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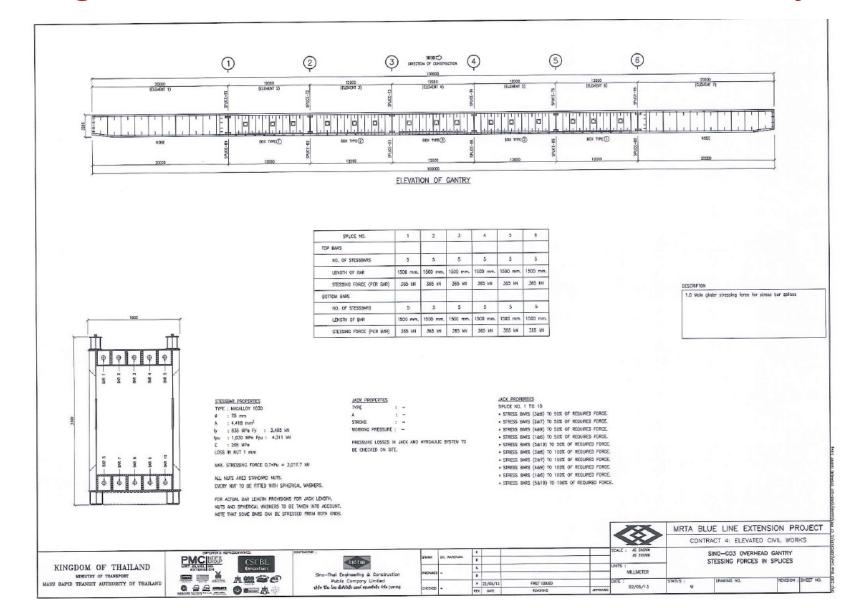






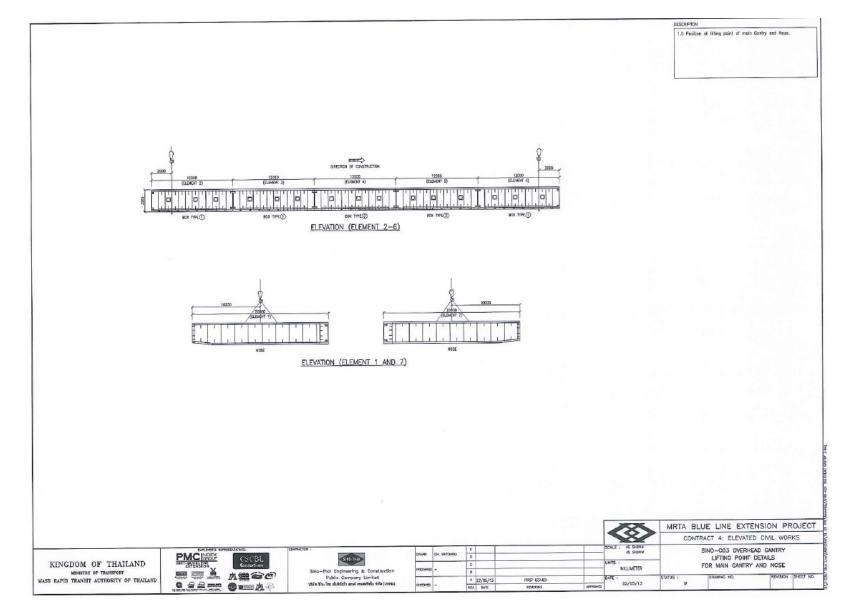






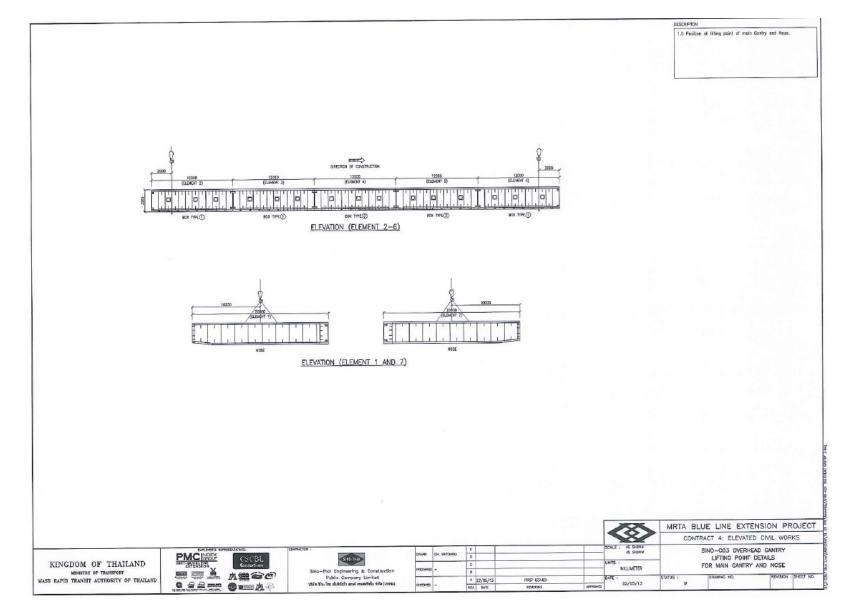






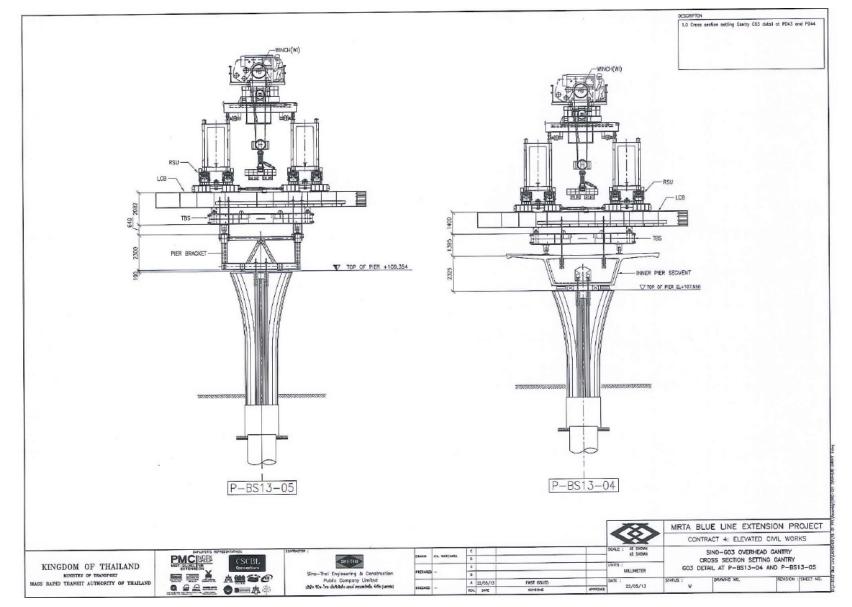






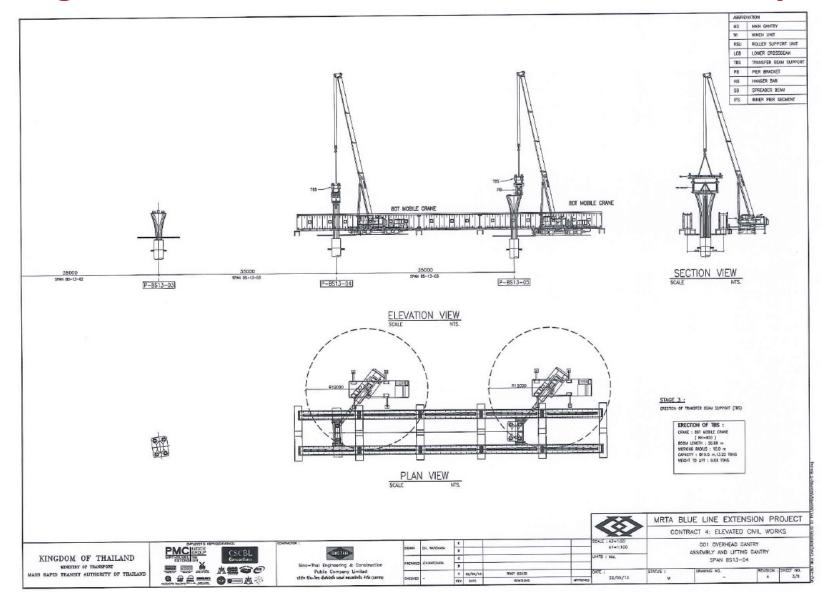








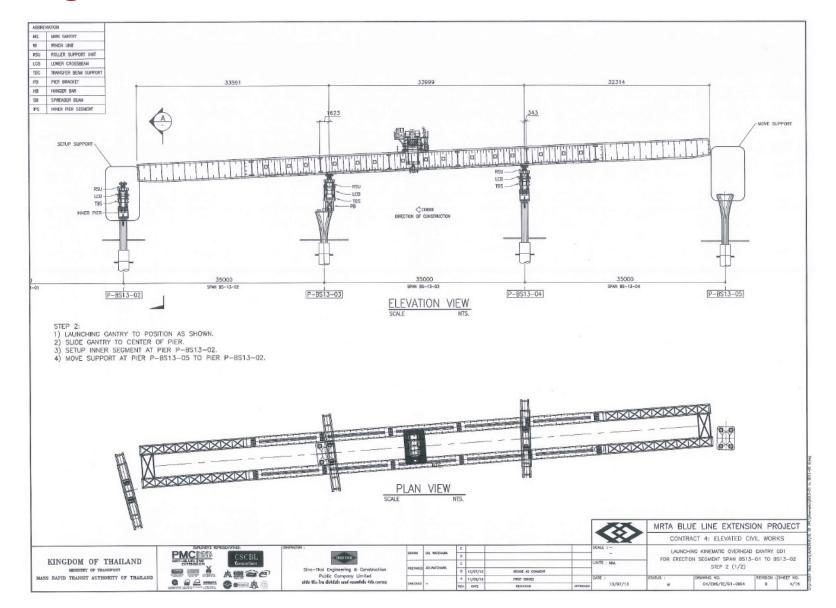








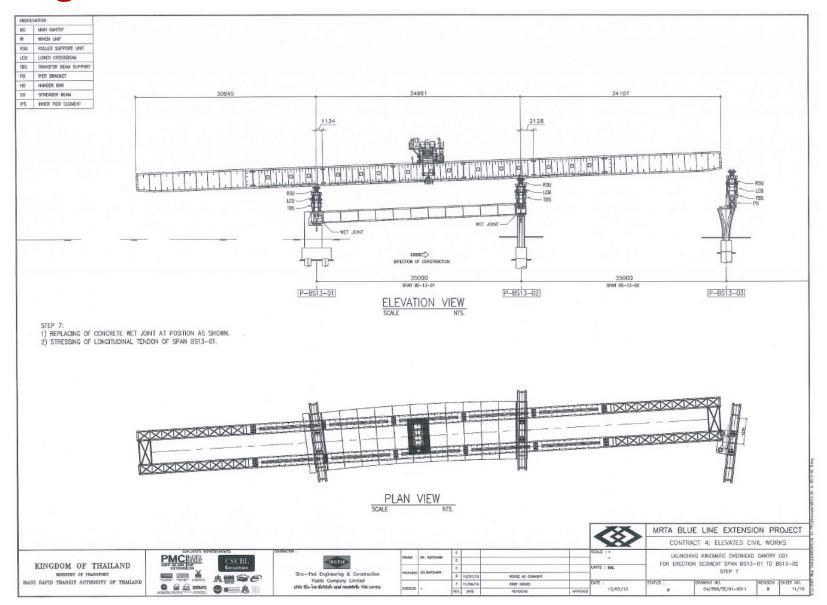
Precast Segmental Box-Girder: Launcher - Kinematic







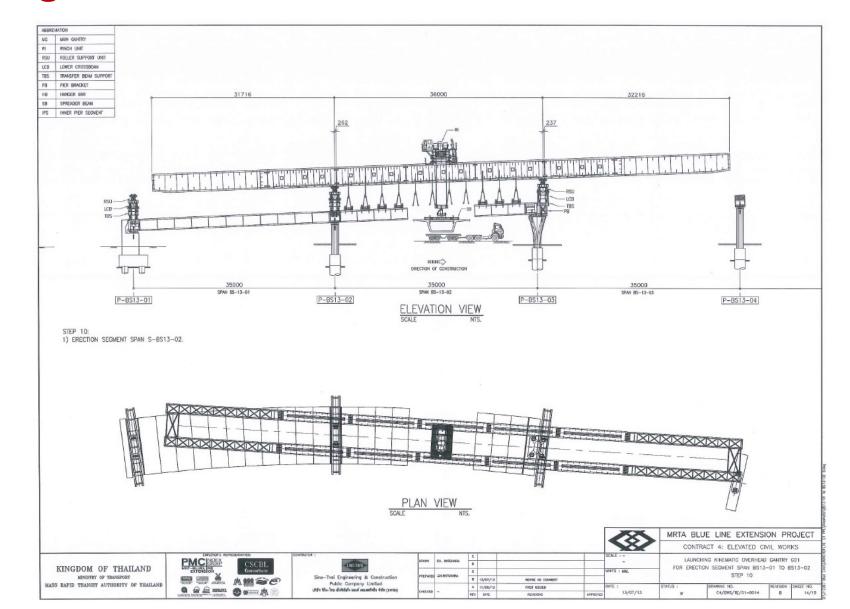
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Precast Segmental Box-Girder: Launcher - Kinematic





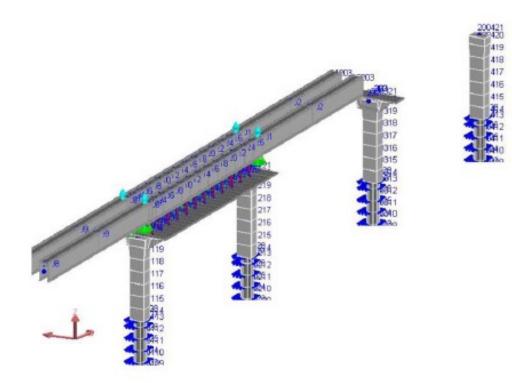


Precast Segmental Box-Girder: Erection Load Transfer

CALCULATION OF LOAD TRANSFER BY OVERHEAD GANTRY

CONTINUOUS 3 SPAN (DT 35-35-35): Follow PT profile at Contract Dwg.

[DRAFT]



Checked Summary

The load transfer procedure was done as recommend step by force on hanger bars and box girder stress result within allowable limit. It shall be notes that, the bottom tensile stress of box girder larger than allowable limit during erecting span 2. Thus for reducing excessive tensile stress, for erecting span2 we recommend to use temporary PT force anchor between pier axis2 to deviator4 of span 2.

Load Transfer Procedure: SPAN 1 (35 m)

- 1.1 Lift up segments and hang to suspension bars.
- 1.2 Aligning and joining segments to final position.
- 1.3 Apply temporary force to closed segment and the shimming in wet joint.
- 1.4 Cast wet joint.
- 1.5 Initial Stressing of tendon T1 to 5% of specified stressing force.
- 1.6 Release the temporary force and the shimming in wet joint.
- 1.7 Stressing of tendon T1 to 25% of specified stressing force.
- 1.8 Stressing of tendon T1 to 100% of specified stressing force.
- 1.9 Stressing of tendon T2 to 100% of specified stressing force.
- 1.10 Lower Gantry by release jacks force at each step 10% from record pressure.
- 1.11 The span is fully load transferred from Gantry on to span support jacks.
- 1.12 Remove all hanger bars and connection beams.





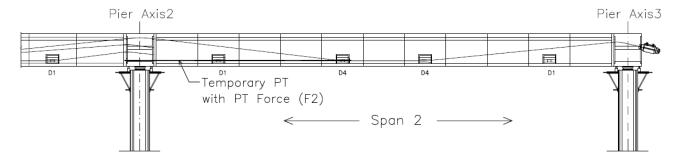
Precast Segmental Box-Girder: Erection Load Transfer

Load Transfer Procedure: SPAN 2 (35 m)

- 2.1 Lift up segments and hang to suspension bars.
- 2.2 Aligning and joining segments to final position.
- 2.3 Apply temporary force to closed segment and the shimming in wet joint.
- 2.4 Cast wet joint.
- 2.5 Initial Stressing of tendon T3 to 5% of specified stressing force.
- 2.6 Release the temporary force and the shimming in wet joint.
- 2.7 Stressing of tendon T3 to 10% of specified stressing force.
- 2.8 Stressing of Temporary force(F2) with 2-PT Bar Between Pier Axis2 to Deviator(D2) of span 2 (Apply force on PT-Bar= 800 KN/ EA)
- 2.9 Stressing of tendon T3 to 50% of specified stressing force.
- 2.10 Stressing of tendon T3 to 100% of specified stressing force.
- 2.11 Stressing of tendon T4 to 100% of specified stressing force.
- 2.12 Lower Gantry by release jacks force at each step +10% from record pressure.
- 2.13 The span is fully load transferred from Gantry on to both pier segment.
- 2.14 Remove all hanger bars and connection beams.

Load Transfer Procedure: SPAN 3 (35 m)

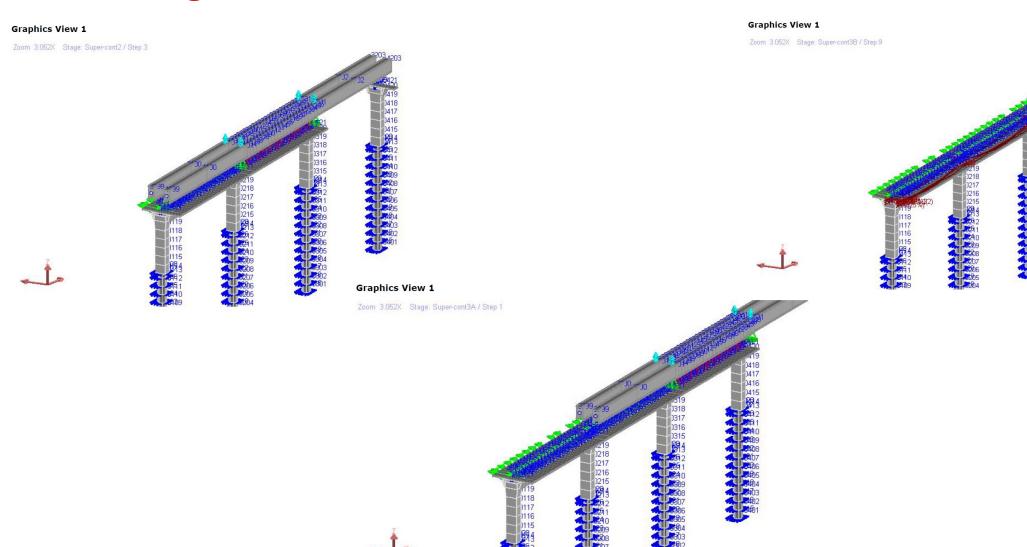
- 3.1 Lift up segments and hang to suspension bars.
- 3.2 Aligning and joining segments to final position.
- 3.3 Apply temporary force to closed segment and the shimming in wet joint.
- 3.4 Cast wet joint.
- 3.5 Initial Stressing of tendon T4' to 5% of specified stressing force.
- 3.6 Release the temporary force and the shimming in wet joint.
- 3.7 Stressing of tendon T4' to 25% of specified stressing force.
- 3.8 Stressing of tendon T4' to 100% of specified stressing force.
- 3.9 Stressing of tendon T2' to 100% of specified stressing force.
- 3.10 Remove Temporary PT Bar at Span2
- 3.11 Lower Gantry by release jacks force at each step 10% from record pressure.
- 3.12 The span is fully load transferred from Gantry on to span support jacks.
- 3.13 Remove all hanger bars and connection beams.
- 3.14 Stressing of tendon T1', T3' to 100% of specified stressing force.
- 3.15 Completed span Erection.







Precast Segmental Box-Girder: Erection Load Transfer









Summary Report

Load Testing of Erection Gantry G01 for MRT Purple Line Project [P044, P043]

4/29/2011



Figure A.2 Installing segment 1,2,3







Figure A.5 Install segments 1, 2, 3, 10, 11, 12 then 4,5 (opposite side)



Figure A.6 Complete span assembly





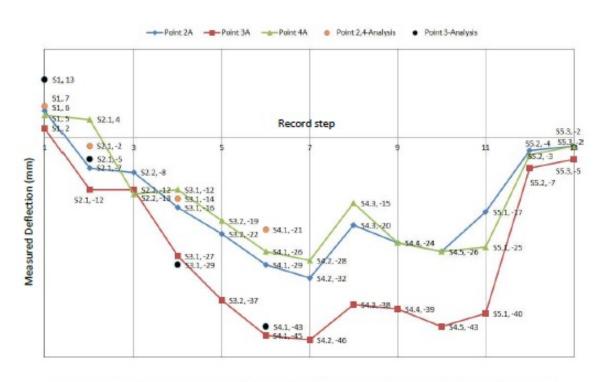


Figure 3.7 Plots of measured deflection and analysis results for each construction stages for Main gantry A

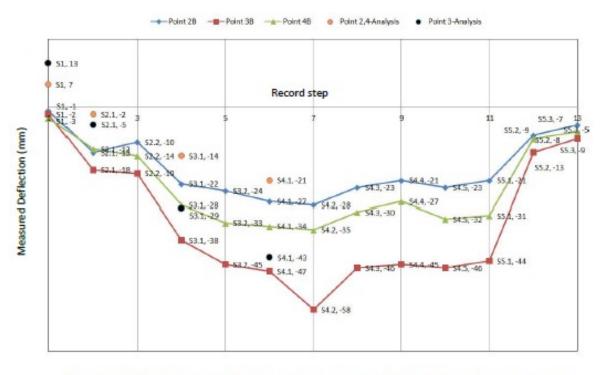
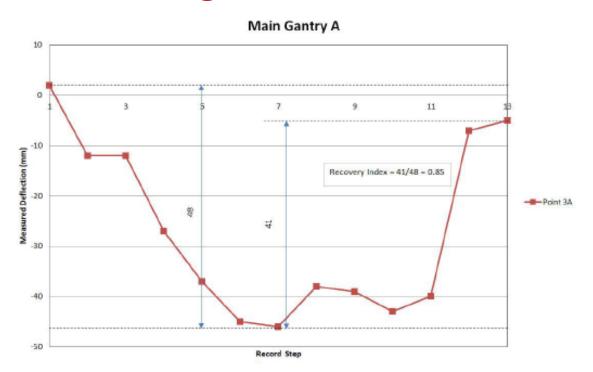


Figure 3.8 Plots of measured deflection and analysis results for each construction stages for Main gantry B

Deflection measurement at each Load Step of Gantry A & Gantry B







Main Gantry B

Recovery Index = 49/56 = 0.88

-50

Record Step

Figure 4.1 Calculation of recovery index for gantry A

Figure 4.2 Calculation of recovery index for gantry B

Recovery Index = Maximum deflection amplitude referred to final loading state

Maximum deflection amplitude referred to initial loading state

Calculation of recovery index for main gantry A and B can be shown in Figs. 4.1 and 4.2, respectively. According to the testing results, the recoverty index for both main gantry is greater than 0.85 (85%).





Precast Segmental Box-Girder: Launcher Operation

When start operating Launcher STECON has process to check and corrective missing and human error of erection works by using 3 separated team with witness point of work to cross check and review process of works before 3 main step of erection works

	. ≪SINO-TI	101>	A CONSTRUCTION PUBLIC COMPANY	-				
			E PROJECT BANG YAI T		JRANA		_	
			J TO BANG SUE SECTION : CONTI					
		การตรวจ	สอบก่อนช่วงการติดตั้งSe	egment				
Name	of Launcher :	G1 Location : P032	- P031 (SPAN_031R) Check Da	ite :1	0/10	, / 2	554	
ลำดับ	2	รายละเอียด		ผลการต	รวจสอบ ไม่ผ่าน	ลายเข็น ผัตรวจ	ข้อคิดเห็น	
1	Main girder			-		gnest		
-	- ตรวาสอบช่องว่างระหว่าง Main girder ที่ประกบติดกัน (connection joint)			-				
_	- ตรวจสอบการโก่งตัวของ Main girder			1				
2	Winch Unit	THE STATE OF THE S		-				
۷.		ในลของระบบไฮโดรลิก		,				
	- ตราจเซ็ลสภาพสายให้ ผู้คอนโทรล							
	- หรางเขียดเกาะหลายเก ผูคอนเกรส - หรางเขียดลักตามจุดร้อย่อย่างๆ							
)—	- สราจเริกสภาพลาดสลิง & wedge socket							
	- ตราจเขตสภาพสายสลง & wedge socket - ตราจสอบสภาพและตำแหน่งของสุดล้อWinch unit					-		
	- ตรวจสอบสภาพและตาแหมงของจุดตองงาควา unit - ตรวจสอบสภาพรอกและสุด			/				
				/		1		
3	ชุดปรับระดับSegment - ตรวจลอบข้อต่อ จุดยึดและสายของระบบไฮโดรลิกของชุดปรับระดับSegment					-		
	 - ตรวจสอบรอดิอ จุดยัดและสายของระบบเอเดรลาของสุดบรบระดบSegment - ตรวจสอบสลักดำงๆของสุดปรับระดับSegment 			/		-		
		กงๆของชุดบรบระดบSegment		/				
4	Hanger Bar							
	- ตรวจสอบสภาพและการโก๋งจรของBarex bar			1		5	26	
	- ตรวจสอบสภาพและการประกอบสุดกระโหลก(Suspension device)			/		1/2	- 1	
	- ตรวจสอบสภาพของลวดSling โดยเฉพาะรอยที่เกิดจากการArc			/		/	, , , , , ,	
	- ตรวจสอบสภาพปลอกอะลูมิเนียมและหัวใจของชุด Sling			/		10/	10/54	
5		Spreader Beam						
	- ตรวจเช็คสภาพ	- ตรวจเช็ดสภาพโครงสร้างและรอยเชื่อมของหูยก						
	- ตรวจเขียสภาพLifting bar(B-B bar) & Anchor Nut			/				
6	Lower Cross B	eam						
	- ตรวจตอบB-B barที่ยึดระหว่างLower cross beamกับTower support:Type-2 ติดตั้งแน่นหรือไม่(ชุดSupportติดตั้งบนEnd pier segment:Single track)						2 more our John	
	ดดดงแนนหรอเม(ชุดธบฤติการต่องานยก pier segment single track) - ตรวจสอบ B-B bar ที่ยึดระหว่าง Lower cross beam กับ Transfer beam และ						Beam support	
	Beam Support Frame ติดตั้งแน่นหรือไม่(ชุดSupportตั้งบนเลาCrossBeam)				119		Way to 12 (3 WK)	
	- ตรวจสอบ B-B bar ที่ยึดระหว่างLower Cross Beamสองท่อนที่ต่อชนกัน			/				
7	Bracket Suppor	rt : Type-2 (ชุด Support ติดตั้งบ	นเต้า Cross Beam)					
	- ตรวจสอบ B-B bar ที่อีด Bracket Support กับ Cross Beam ติดตั้งแน่นหรือไม่			/				
8	Beam Support	Beam Support Frame (ชุด Support ติดตั้งบนเล่า Cross Beam)					Deam Support	
	- ตรวจสอบความนั้นคงของBeam Support Frame				/		Fogure of Tolor	
	- ตรวจสอบLock กบเของไฮโดรลิกแจ็คที่ค้ำLCBถูกขันส็จกแล้วหรือไม่				-		M)	
2-15-17	Launcher Engineer QC Engineer				PojeorEngineer			
Sign		6	Eggins 8 2758	8		VX.		
Name-Surname Charles Ons		energ andre	निकार क्रियाच्या व्यवस्था		560	25000 prom		
	Date	10/10/54	10/10/12		1	16/14	100	
รถรำลักเร	ายการด้วนหน้ได้รับ	การตรวจสอบและดำเนินการครบถ้ว				100	17.	

Check before erection

การตรวจสอบก่อนช่วงการLaunch Main girde Location : 1001-100 To Spon Obje Check Date : Tower Support (ชุดSupportติดตั้งบนEnd pier) ตรวจสอบสภาพข้อต่อและสายของระบบไฮโดรลิกที่ต่อเข้าแจ็กของชุดTower ตรวจตอบ Lock nut ถูกขันด็ชกระดับความสูงของแจ็ค Tower support แล้ว ตรวจสตบการขันติดตั้ง Stud bar ชื่อระหว่าง Tower support กับ End pier ament ในกรณี Tower support วางติดตั้งบน End pier segment) ransfer Beam : Type-2 (ชุด Support ติดตั้งบนเสา Cross beam) ครวงสอบสภาพข้อต่อและสายของระบบไฮโดรลิกที่ต่อเข้าแจ็คของชดTower ตรวจสอบ Lock nut ถูกขันลีอกระดับความสูงของแจ็ค Tower support แล้ว ตรวจสอบ B-B bar ที่ขีดระหว่าง Transfer Beam กับ Bracket Support ติดตั้ง Transfer Beam : Type-3 (ชุด Support ติดตั้งบนเลา Cross Beam) ตรวจสอบ B-B bar ที่ยึด Transfer Beam Support กับ Cross Beam ติดตั้ง ตรวจสอบฐานของ Transfer Beam Support วางแนบสนิทกับชุดShimหรือ ตรวจสอบ Lock nut ถูกขันส็อกระดับความสูงของแจ็ค Transfer Beam ตรวจสอบ B-B bar ที่ยึดระหว่าง Transfer Beam กับ Lower Cross Beam Note: เพื่อเลิช รือ ๆ ๆเมเตอาไฮโลรัสเเลิล สังเ LCB ไม่รั้งกา อยู่ 1 gon ช Pia co (ปังกอลก) (แล้วให้กมาแกงแห้น เรื่อ Smil Frank

Check before Launching

	มรินัก ซีโน-ไทย เช็นซีเนียริง แอนค์กอนสทรักชั้น จักกัด (มหา: sno-malenginzering a construction public company limit								
	MRT PURPLE LINE PROJECT BANG YAI TO RA	T BURA	NA		-				
	BANG VAI TO BANG SUE SECTION: CONTRACT 2								
	การตรวจสอบก่อนช่วงการSlide Mair	Girder							
Name	of Launcher: 61 Location: POSS-POSS (SPAN 032 E Ph	eck Date :	4/	10/3	1554				
ลำตับ	รายละเขียด		ผลการตรวจต่อบ		ข้อคิดเห็น				
1	***	ผ่าน	ไม่ผ่าน	ผู้ตรวจ	DOTTELLIS				
	Main girder		_	1					
	- ตรวจสอบเก็บสายไฟขึ้น Main girder ให้เรียบร้อย	/							
	- ตรวจสอบจัดเก็บสิ่งของหรืออุปกรณ์บน Main girder ที่อาจล่วงหล่นลงคู่ด้านล่าง	1							
!	Winch unit								
	- ตรวจสอบตำแหน่งจอดของ Winch Unit อยู่กึ่งกลางช่วง Span	1							
3	Roller Support								
	ตรวจสอบจะต้องมีสลักยึดระหว่าง Brake Launching jack หรือ Main								
	Launching jack ปิดกับ Launching rail อย่างใดอย่างหนึ่งเป็นอย่างน้อย	/							
	ตรวจสอบสลักและสภาพของชุด Spindle ที่ยึดระหว่าง Roller Support	/							
	ตรวจสอบ Main girder นั่งอยู่บนล้อของสุด Roller Support ในทุกๅจุด	1							
	ตรวจสอบสภาพกระบอกไฮโดรติก รวมถึงสภาพข้อต่อและสายที่ใช้ในการเลื่อน	-							
	Slide ตัว Main girder	/							
	ตรวจสอบสภาพหูและ B-B bar ที่ใช้ในการดึง Slide ตัว Main Girder	-		> 1	29				
	ตรวจสอบแผ่นTellonแนบสนิทกับแผ่นStainlessของLCBทุกจุดรวมถึงสภาพ	/		1/1					
_	ของแผ่นTeflon	/		4/1	0/54				
_	Lower Cross Beam								
	ตรวจสอบความสะขาดของแผ่นStainless รวมถึงการชโดมน้ำมันหล่อลื่น	/							
-	ตรวาลอบจุดรอยต่อและสภาพความเรียบของแผ่นStainless		/	6-	VIANCOS				
-	ตรวจสอบ B-B bar ที่ยึดระหว่าง Lower cross beam กับ Tower support		-						
ĝ	คตั้งแน่นหรือไม่(สุด Support ตั้งบน End pier)	/	- 1/						
-	ทรวจสอบ B-B bar ที่อีดระหว่าง Lower cross beam กับ Transfer beam และ			-	,				
	eam Support Frame ติดตั้งแน่นหรือไม่(ชุดSupportตั้งบนCrossBeam)	/	- 11						
-	สรวจสอบความมั้นคงของชุดราวกันตกตัวLower cross beam	,		-					
	เรวจสอบจัดเก็บสิ่งของบนทางเดินบน Lower cross beam ที่อาจก็ดขวาง	-		7	edandan				
4	งเวลาท้างาน .		/		1 00 m				
- 1	รวจสอบ B-B bar ที่ยึดระหว่างLower Cross Beamสองพ่อนที่ต่อชนกัน	/		L	rului da				
			H	1	and an elo				
	Launcher Engineer QC Engineer		1	ject Engine	er				
Si	in Jarries Happe	1/2/2							
Name-Surname Wish Gurdon 900 0000 00000		Sonie month							
Da		-	7	,	10/54				

Check before sliding

s.athasit@gmail.com





Precast Segmental Box-Girder: Launcher Operation



Launching



Span Alignment & Profile check



Concrete wet joint



Erection



Post-Tensioned works





Thank you Question & Answer