

# Importance of Earthquake-Related Detailing in Construction:



## Experiences from the Mandalay Earthquake in Myanmar

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27<sup>th</sup> June 2025  
Bangkok, Thailand

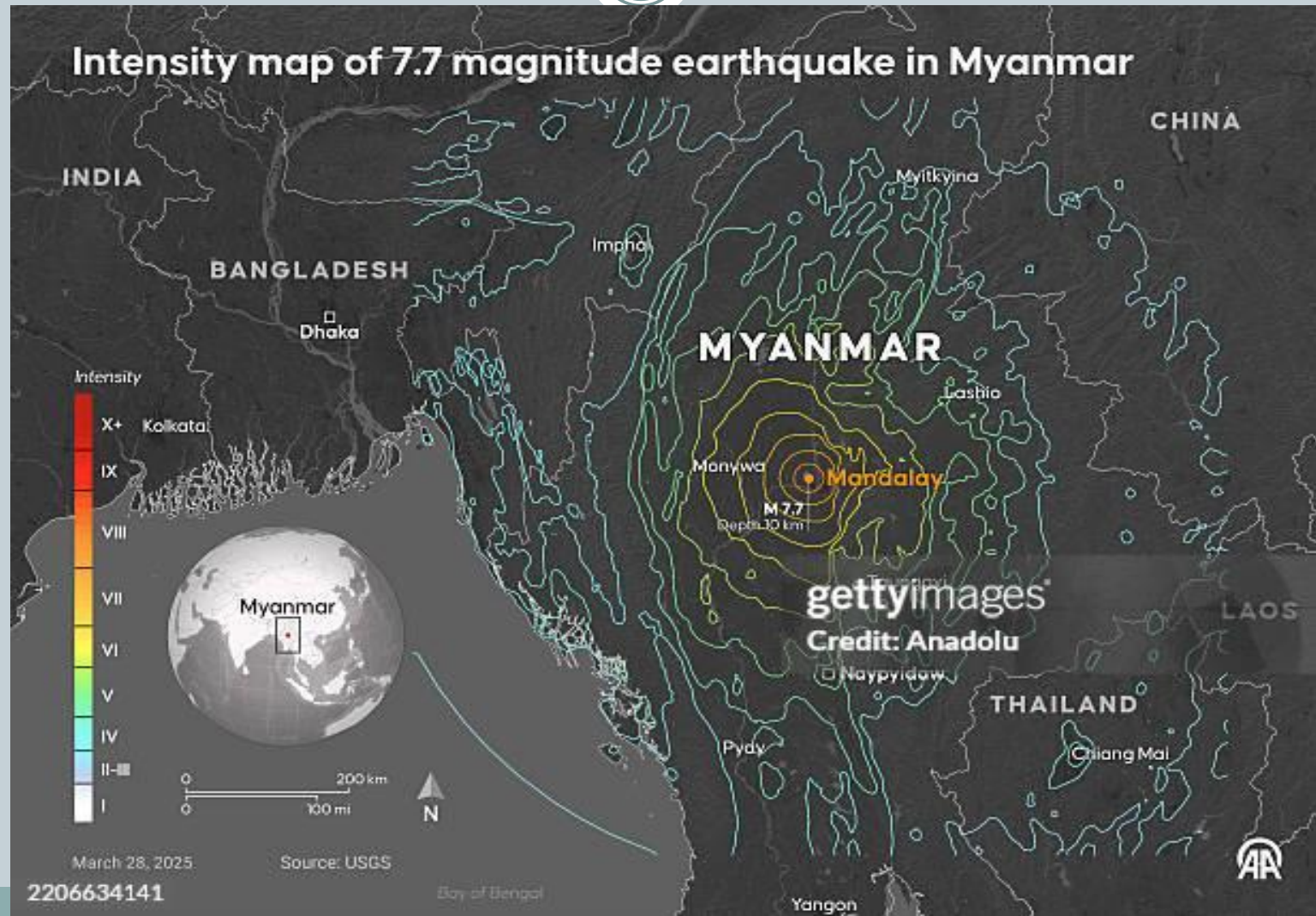
# Background



- 28 March 2025 at 12:50:52 [MMT](#) (06:20:52 UTC), a Magnitude 7.7 [earthquake](#) struck the [Sagaing Region](#) of Myanmar, with an [epicenter](#) close to [Mandalay](#), the country's second-largest city.
- It was the most powerful earthquake to strike Myanmar since [1912](#), and the second deadliest in Myanmar's modern history, surpassed only by upper estimates of the [1930 Bago earthquake](#).
- The earthquake caused extensive damage in Myanmar and significant damage in neighboring Thailand. Hundreds of homes were also damaged in [Yunnan](#), China, while more than 400 apartments were affected in [Ho Chi Minh City](#), Vietnam. ( Ref . : Wikipedia.)

the Sagaing Fault, a major transform fault within Myanmar, a significant source of seismic activity.

The Sunda megathrust, a major fault line, runs along Myanmar's western coast, capable of generating large earthquakes caused by subduction of the Indian plate beneath the Burma plate.





**MODIFIED MERCALLI INTENSITY SCALE (MMI) AFTER USGS**

<b>Intensity</b>	<b>Shaking</b>	<b>Description/Damage</b>
I	Not felt	Not felt except by a very few under especially favorable conditions.
II	Weak	Felt only by a few persons at rest, especially on upper floors of buildings.
III	Weak	Felt quite noticeably by persons indoors, especially on upper floors of buildings. Many people do not recognize it as an earthquake. Standing motor cars may rock slightly. Vibrations similar to the passing of a truck. Duration estimated.
IV	Light	Felt indoors by many, outdoors by few during the day. At night, some awakened. Dishes, windows, doors disturbed; walls make cracking sound. Sensation like heavy truck striking building. Standing motor cars rocked noticeably.
V	Moderate	Felt by nearly everyone; many awakened. Some dishes, windows broken. Unstable objects overturned. Pendulum clocks may stop.
VI	Strong	Felt by all, many frightened. Some heavy furniture moved; a few instances of fallen plaster. Damage slight.
VII	Very strong	Damage negligible in buildings of good design and construction; slight to moderate in well-built ordinary structures; considerable damage in poorly built or badly designed structures; some chimneys broken.
VIII	Severe	Damage slight in specially designed structures; considerable damage in ordinary substantial buildings with partial collapse. Damage great in poorly built structures. Fall of chimneys, factory stacks, columns, monuments, walls. Heavy furniture overturned.
IX	Violent	Damage considerable in specially designed structures; well-designed frame structures thrown out of plumb. Damage great in substantial buildings, with partial collapse. Buildings shifted off foundations.
X	Extreme	Some well-built wooden structures destroyed; most masonry and frame structures destroyed with foundations. Rails bent.



# MERCALLI VS. RICHTER

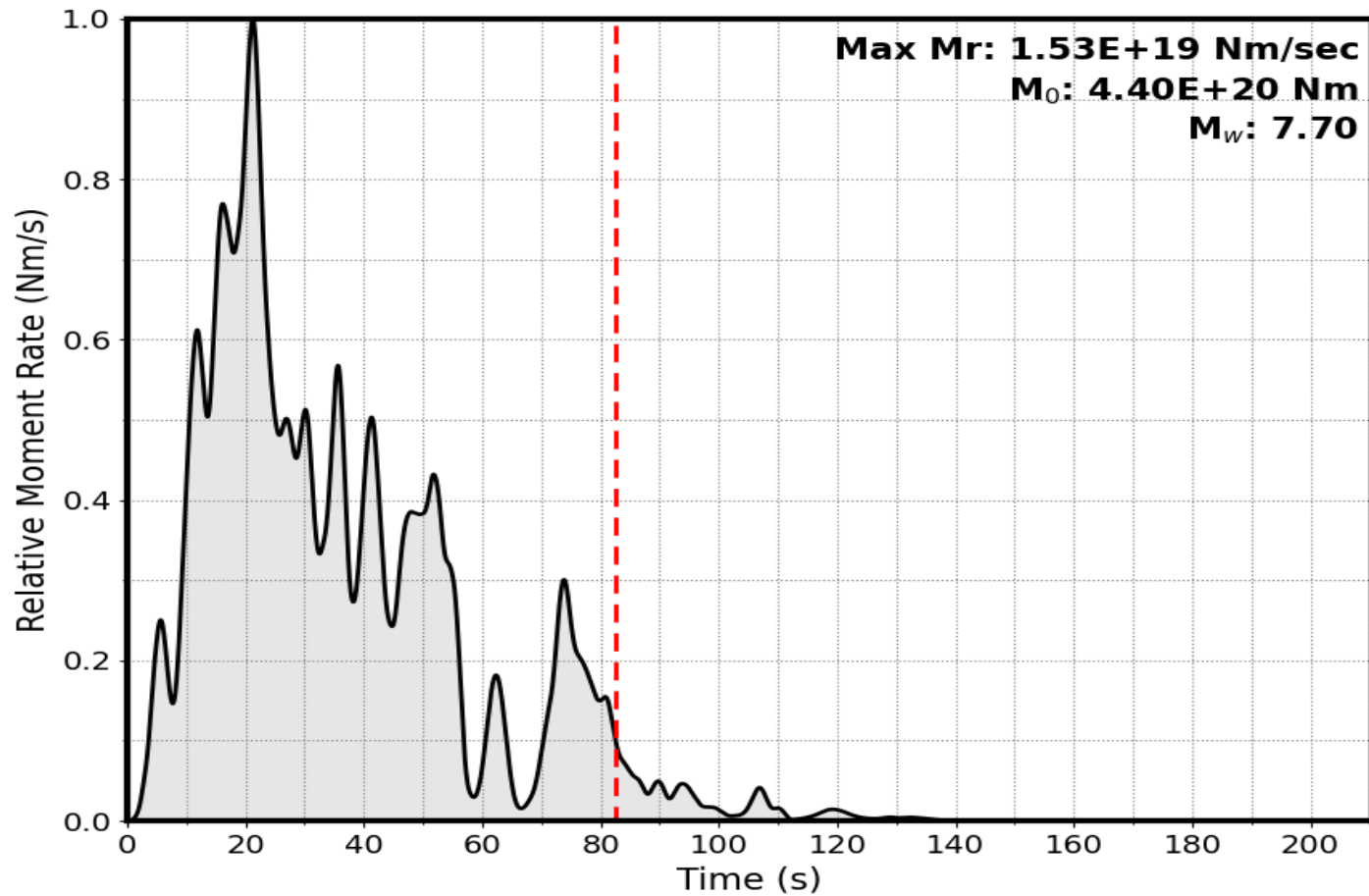
MODIFIED MERCALLI SCALE		RICHTER SCALE	
I.	Felt by almost no one.	2.5	Generally not felt, but recorded on seismometers.
II.	Felt by very few people.	3.5	Felt by many people.
III.	Tremor noticed by many, but they often do not realize it is an earthquake.		
IV.	Felt indoors by many. Feels like a truck has struck the building.		
V.	Felt by nearly everyone; many people awakened. Swaying trees and poles may be observed.		
VI.	Felt by all; many people run outdoors. Furniture moved, slight damage occurs.	4.5	Some local damage may occur.
VII.	Everyone runs outdoors. Poorly built structures considerably damaged; slight damage elsewhere.		
VIII.	Specially designed structures damaged slightly, others collapse.	6.0	A destructive earthquake.
IX.	All buildings considerably damaged, many shift off foundations, Noticeable cracks in ground.		
X.	Many structures destroyed. Ground is badly cracked.	7.0	A major earthquake.
XI.	Almost all structures fail. Very wide cracks in ground.	8.0 and up	Great earthquakes.
XII.	Total destruction. Waves seen on ground surfaces, objects are tumbled and tossed.		

# Overview of Mandalay Earthquake



- • Date: March 28, 2025, 12:50:52 Local Time
- • Magnitude: 7.7
- • Epicenter: Near Mandalay, 22.011°N 95.936°E
- 10.0 km depth
- • Effects: Significant structural damage, casualties, and disruptions.

# Moment Magnitude





# Introduction



- Earthquake-related detailing refers to construction practices that improve seismic resilience.
- Essential in regions prone to seismic activity like Myanmar.
- Prevents catastrophic failure of buildings during earthquakes.

# Types of Damage Observed



- • Collapse of bridges and buildings
- • Cracks in reinforced concrete frames
- • Failure of structural elements
- • Poor performance of unreinforced masonry





# Earthquake induced Lateral Force



# Root Causes of Damage



- • Inadequate detailing in construction
- • Lack of ductile reinforcement
- • Poor quality control
- • Ignoring code provisions
- • Informal construction practices



### Failure of Column in Shear

Improper confinement of longitudinal bars led to shear failure column during earthquake





## Open Ground Storey

Upper storey stiffened by brick walls and less stiffer ground floor

Failure of columns because of poor energy dissipation capacity





Failure of building due to weak column strong beam





Failure of column due to captive effect





Failure of steel frame due to warping torsion

# What is Earthquake-Related Detailing?



- • Ductile design
- • Proper stirrup spacing
- • Beam-column joint reinforcement
- • Confinement reinforcement in columns
- • Ensures energy dissipation during quakes
- • Captive effect due to Architectural Requirements

# Splice Zone in RC Structure For Seismic Consideration

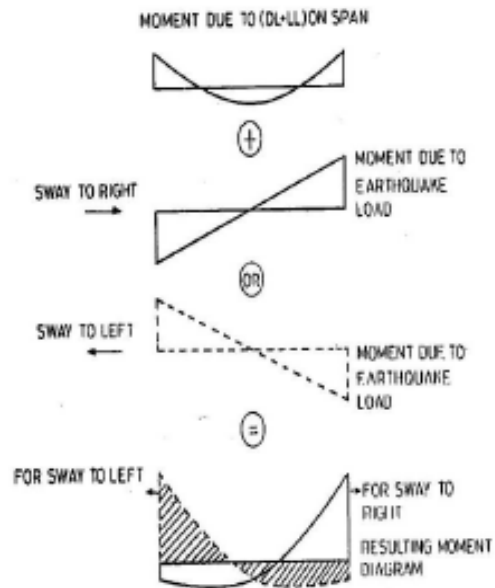


Figure C3 – Reversal of moments due to earthquake loading

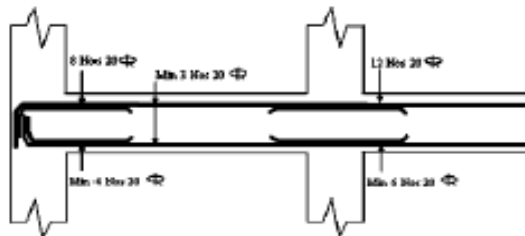


Fig. C4 – Longitudinal reinforcement at the joints in a beam

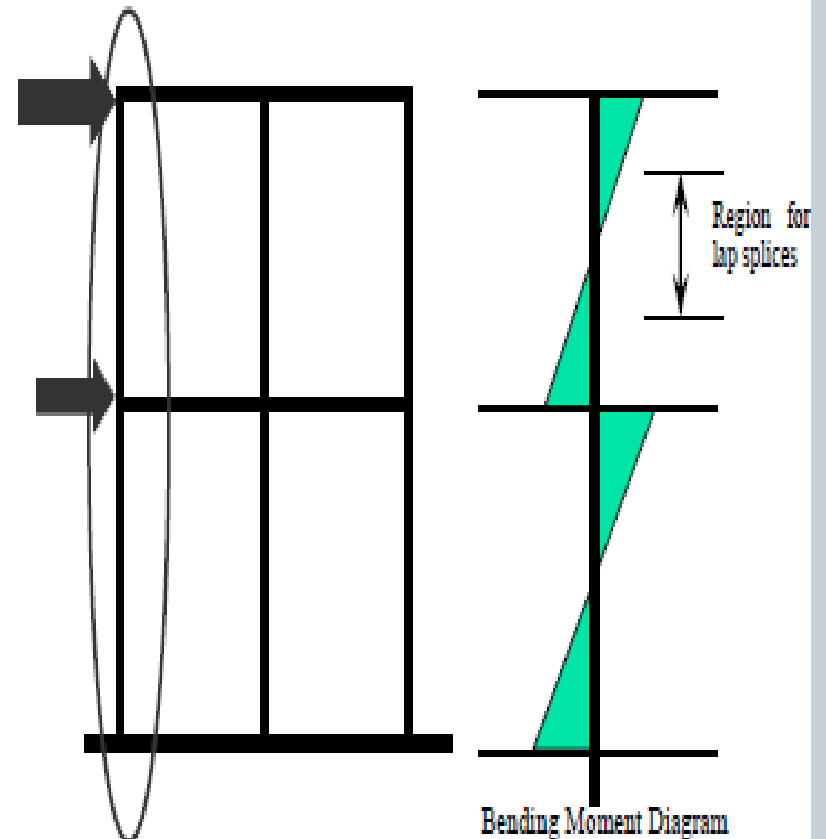


Fig. C7 – Region for lap splices



## **B. ORDINARY & SEISMIC DETAILINGS OF R. C. STRUCTURES**

### **(1) General**

#### **Seismic zones**

**According to UBC (Uniform Building Code),**

Seismic Zones are 0, 1 (Low) ; 2A, 2B (Moderate) ; 3, 4 (High Seismic Risk).

Yangon is considered as in equivalent Zone 2A UBC (Myanmar Zone II/III)

Mandalay is considered as in equivalent Zone 4 UBC (Myanmar Zone V)

[ **Note** : Myanmar Zones are : I, II, III, IV and V – see the Seismic Zone map ]

#### **Moment-Resisting Frames and Detailing Requirements**

- (i) Ordinary Moment-Resisting Frames (OMRF) for Zones 0 and 1 (UBC) —  
require no seismic detailing; ordinary detailing is sufficient
- (ii) Intermediate Moment-Resisting Frames (IMRF) for Zones 2A and 2B (UBC) —  
require detailing for IMRF
- (iii) Special Moment-Resisting Frames (SMRF) for Zones 3 and 4 (UBC) —  
require detailing for SMRF

**Note :** *Dual system and other framing systems are not included in this discussion. Dual system means ( shear wall / braced frame ) + ( OMRF / IMRF / SMRF ) acting together.*



## (2) Ordinary Moment-Resisting Frame Detailing

### Slabs

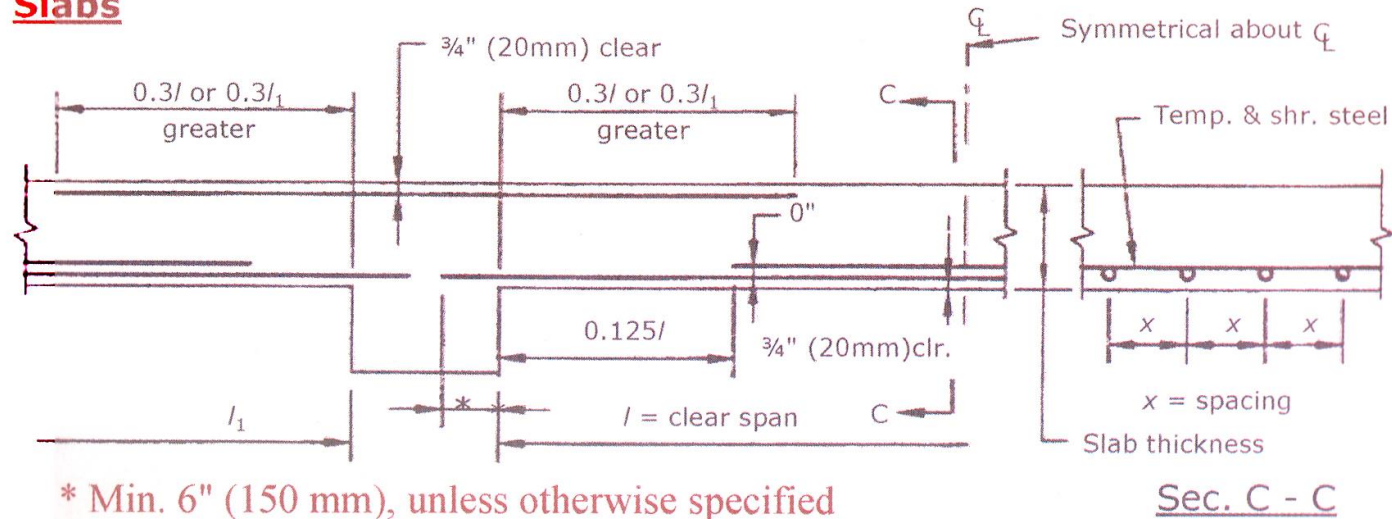


Fig. Interior span, continuous one-way slab

For slabs,

Maximum spacing

=  $3h$  (or) 18" (one-way slab – for main steel)

=  $2h$  (or) 18" (two-way slab – for main steel)

=  $5h$  (or) 18" (for temp. & shr. steel)

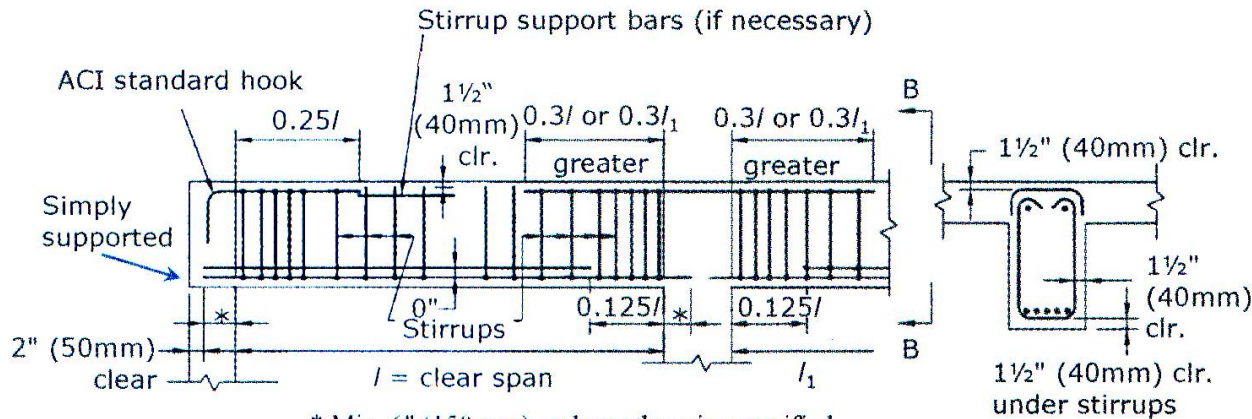
**Note :**  $A_{s,min}$  for slab =  $0.002 bh$  for  $f_y = 40/50$  ksi ( = temp. & shr. steel )

=  $0.0018 bh$  for  $f_y = 60$  ksi ( = temp. & shr. steel )



## (2) Ordinary Moment-Resisting Frame Detailing *contd.*

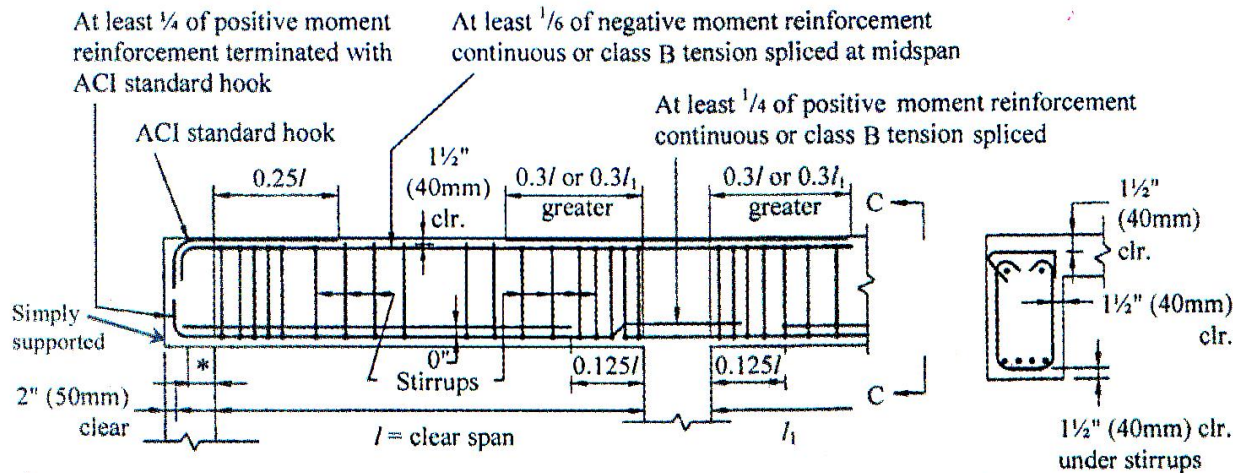
### Beams



**Fig. Non-perimeter beam with closed stirrups**

Sec. B - B

Note : if the end of exterior-span beam is monolithic with R. C. column or shear wall, assume the same as interior-span beam.



**Fig. Perimeter beam**

Sec. C - C

For beams,  
max. spacing of stirrups  
is the smallest of

$$(1) s_{max} = \frac{A_v f_y}{0.75 \sqrt{f'_c} b_w} \leq \frac{A_v f_y}{50 b_w}$$

$$(2) s_{max} = \frac{d}{2}$$

$$\left( = \frac{d}{4} \text{ if } V_s > 4 \sqrt{f'_c} b_w d \right)$$

$$(3) s_{max} = 24 \text{ in.}$$

$$\left( = 12 \text{ in. if } V_s > 4 \sqrt{f'_c} b_w d \right)$$

$$(4) s_{max} = \frac{P_h}{8} \text{ or } 12 \text{ in.}$$

(closed stirrups for torsion case) where  $P_h$  is perimeter of centreline of stirrups.

**Note:**

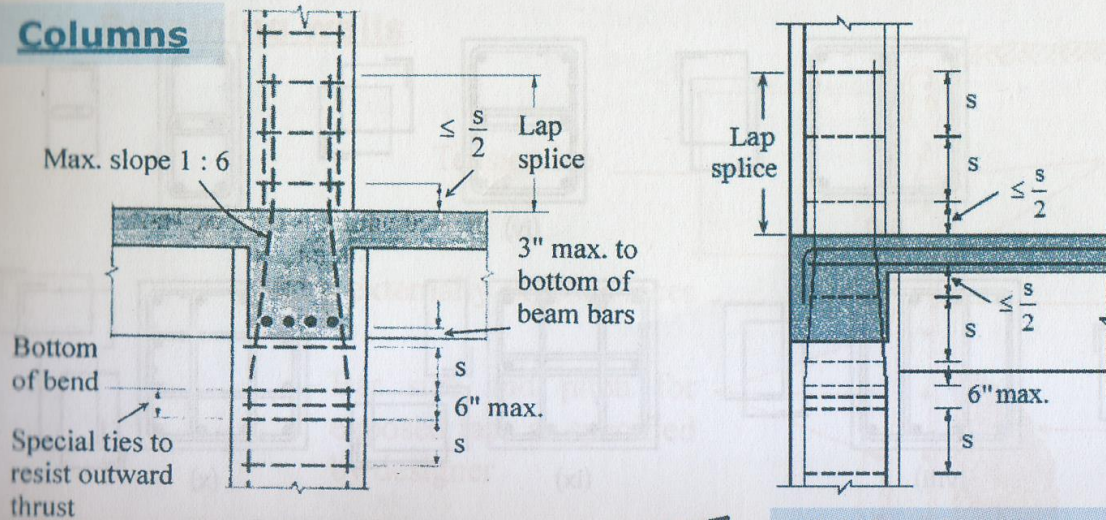
$$\rho_{min} = \frac{3 \sqrt{f'_c}}{f_y} \geq \frac{200}{f_y}$$

**for main steel**



## (2) Ordinary Moment-Resisting Frame Detailing *contd.*

### Columns



(a) Interior column

(b) Exterior column

For tied columns,  
max. spacing is

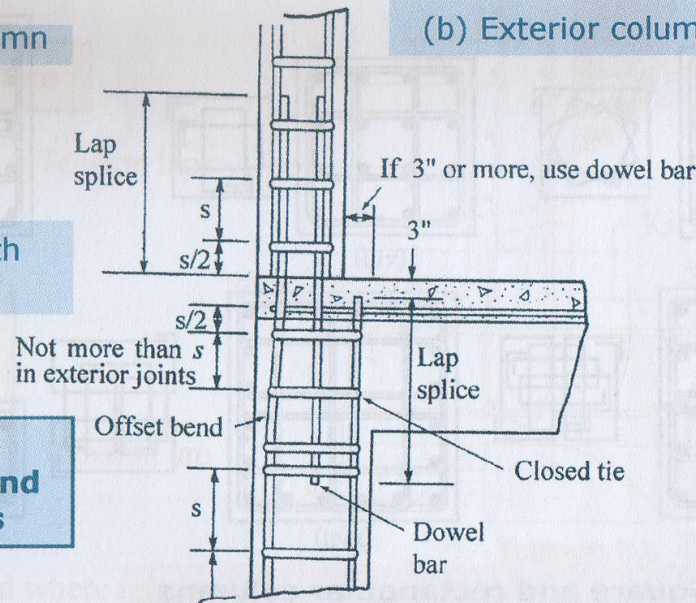
- (1)  $s_{max} = 16 d_b$
- (2)  $s_{max} = 48 d_t$
- (3)  $s_{max} = \text{smaller dimension of column section}$

**Note:** ties at least No. 3 in size; no unsupported main bar shall be farther than 6 in. clear from a supported bar. Lateral support is to be provided by the corner of a tie having an included angle  $\leq 135^\circ$

**Note:**  $\rho_{min} = 0.01$  ;  $\rho_{max} = 0.08$   
for longitudinal bars  
(non-seismic case)

(c) Exterior column with large offset

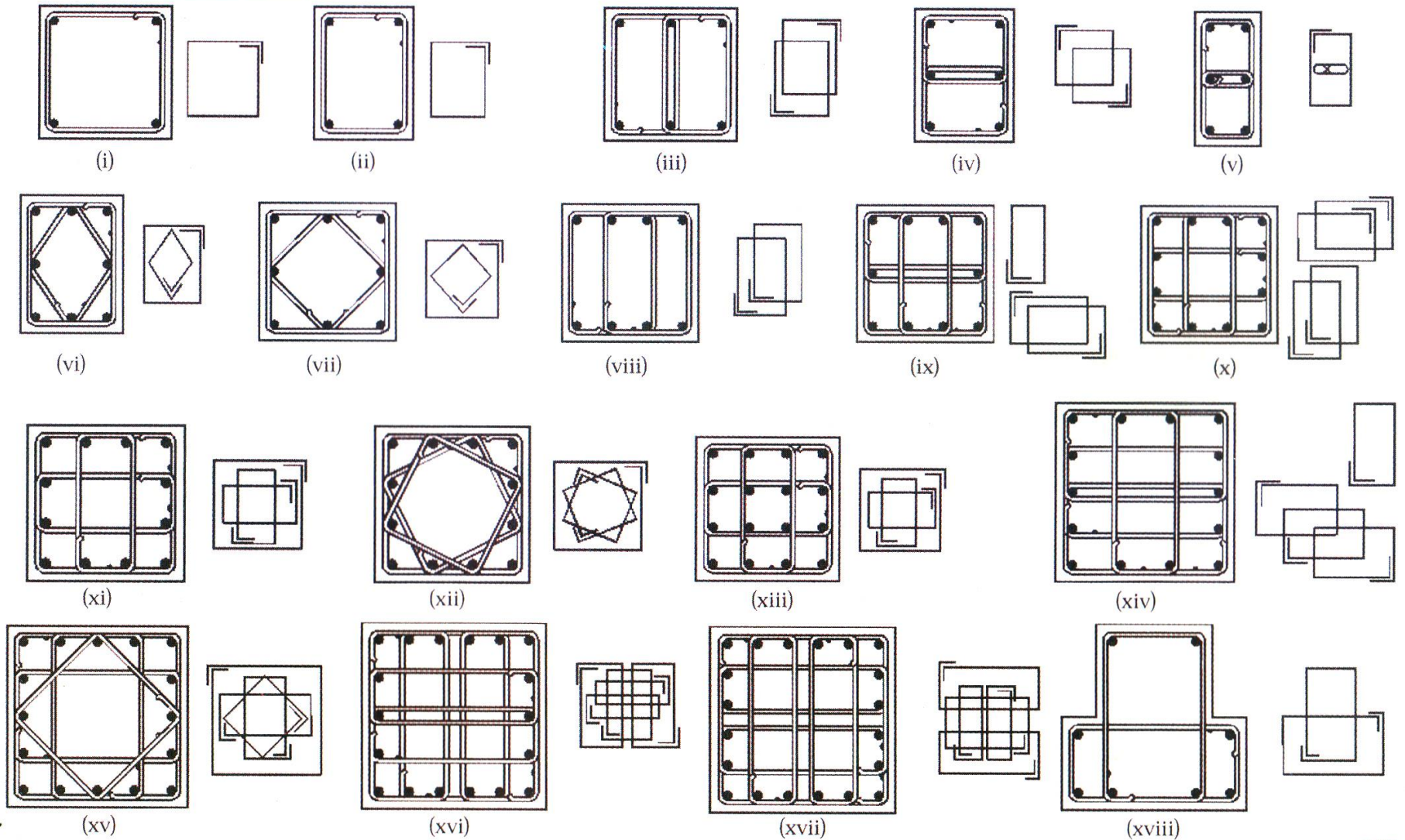
**Fig. Splice details at typical interior and exterior columns**





## (2) Ordinary Moment-Resisting Frame Detailing *contd.*

### Columns *contd.*



**Fig. Square and rectangular columns**



## (4) Intermediate Moment-Resisting Frame Detailing

### Beams

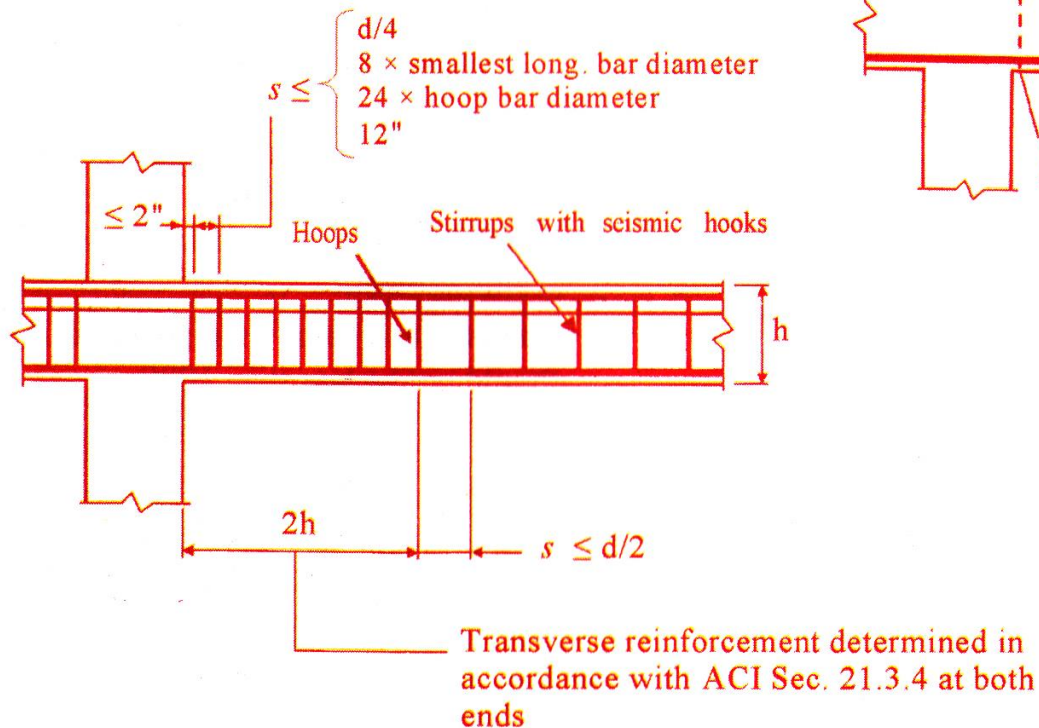
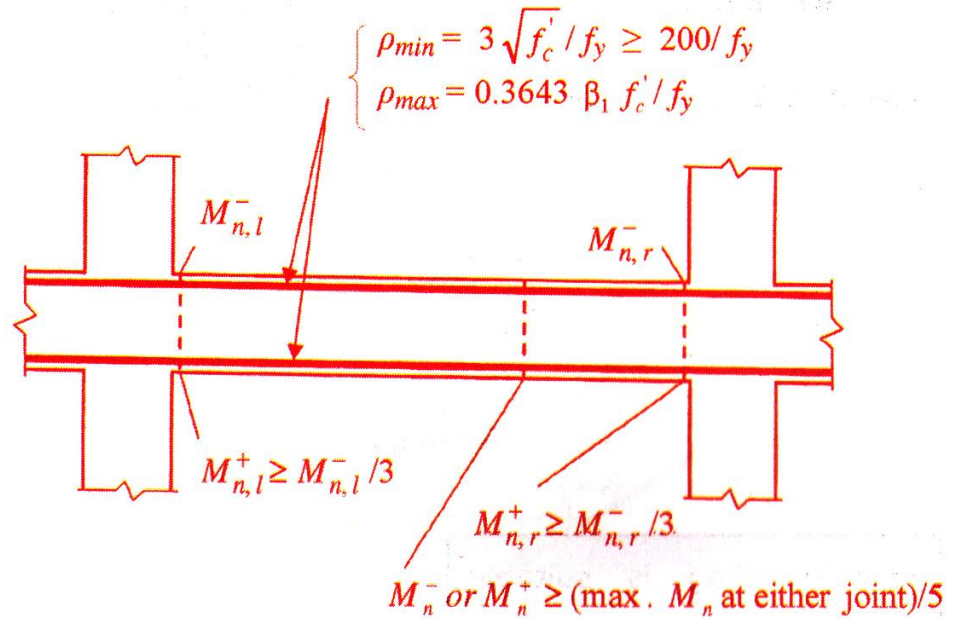


Fig. Transverse reinforcement requirements for beams



Note: Transverse reinforcement not shown for clarity

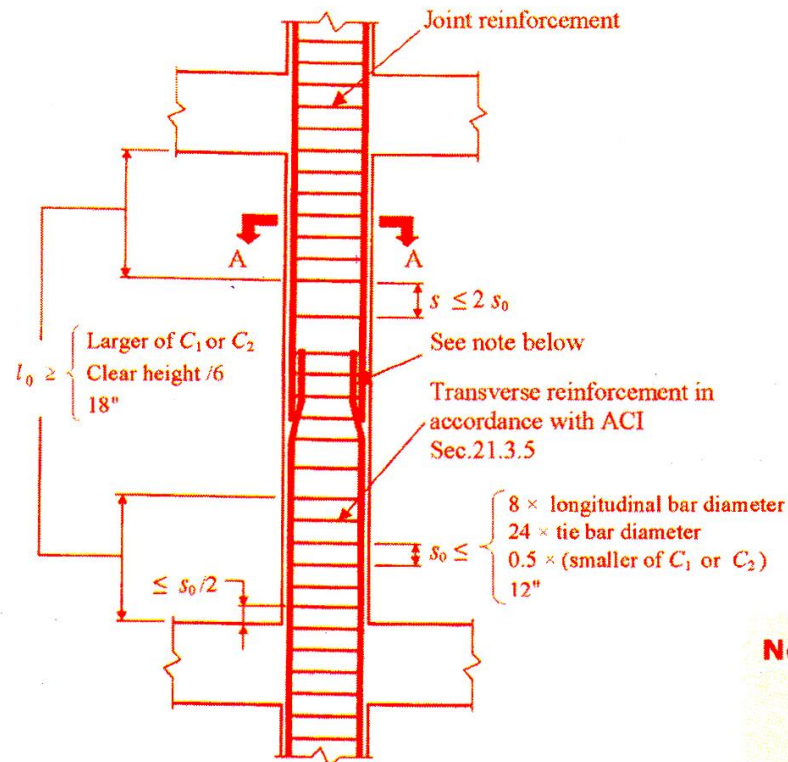
Fig. Flexural requirements for beams

$$\beta_1 = 0.85 \text{ for } f'_c \leq 4000 \text{ psi}$$

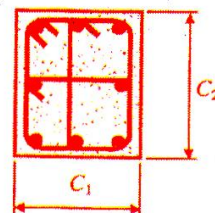
$$= 0.80 \text{ for } f'_c = 5000 \text{ psi}$$

#### (4) Intermediate Moment-Resisting Frame Detailing *contd.*

##### Columns



**Note:** *There is no restriction on the location of longitudinal bar splices for intermediate moment frames. The splice may be located away from the potential hinge regions (i.e., near the joints ) as shown above.*

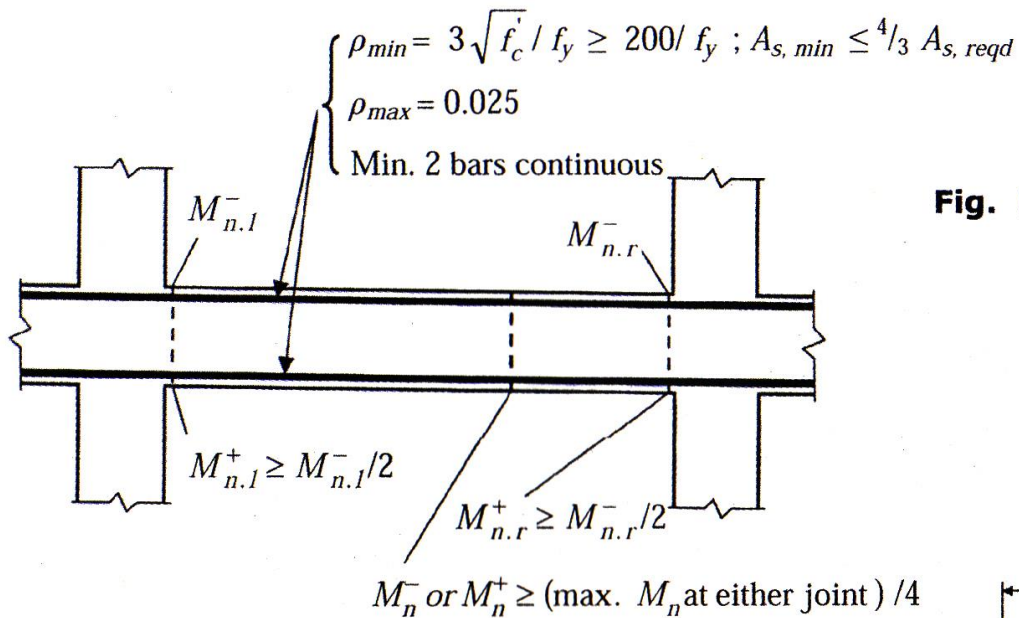


Section A-A

**Fig. Transverse reinforcement requirements for columns**

## (5) Special Moment-Resisting Frame Detailing

### Beams



Note: Transverse reinforcement not shown for clarity

Fig. Flexural requirements for beams

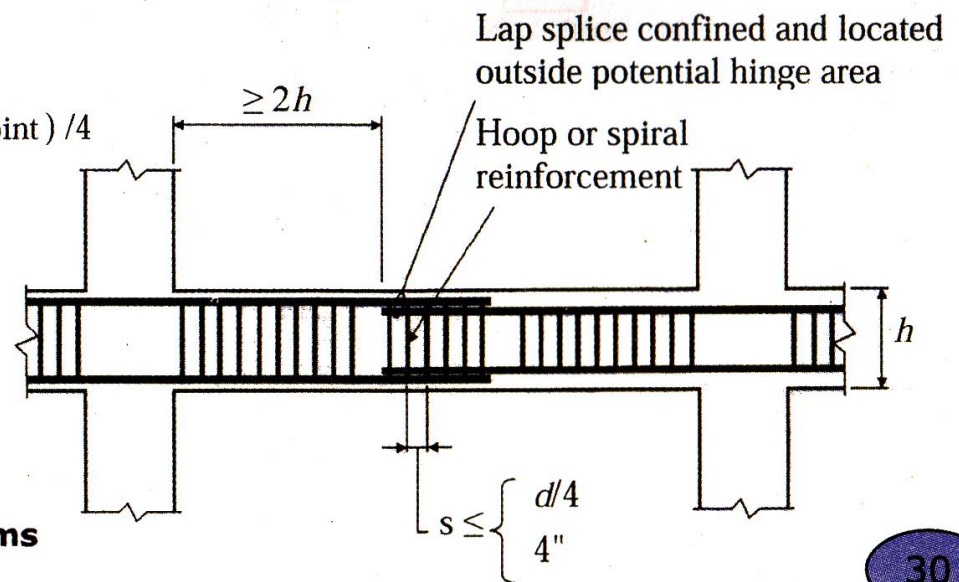
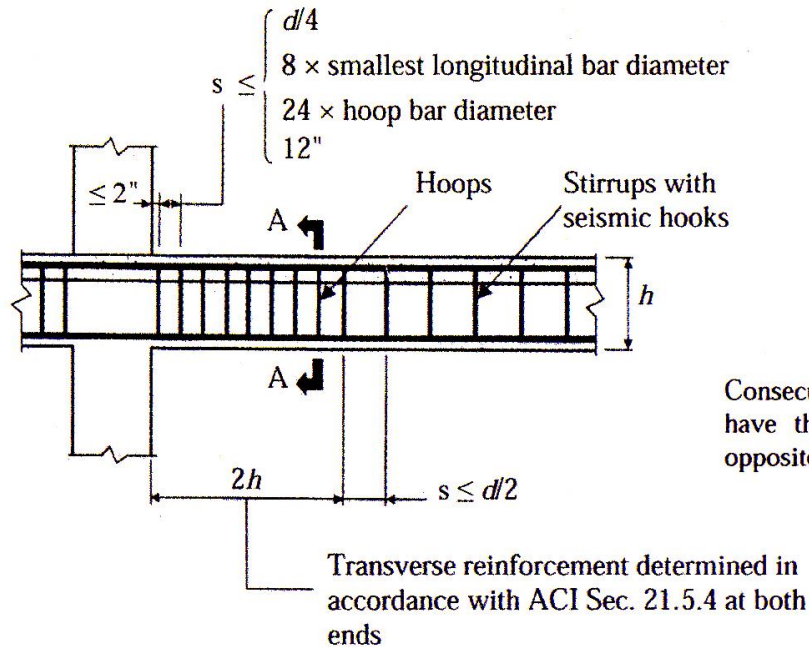


Fig. Lap splice requirements for beams

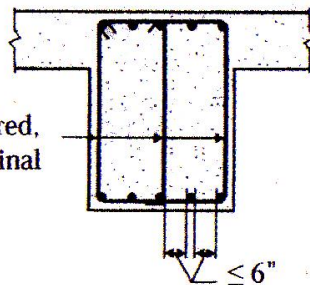


## (5) Special Moment-Resisting Frame Detailing *contd.*

### Beams *contd.*

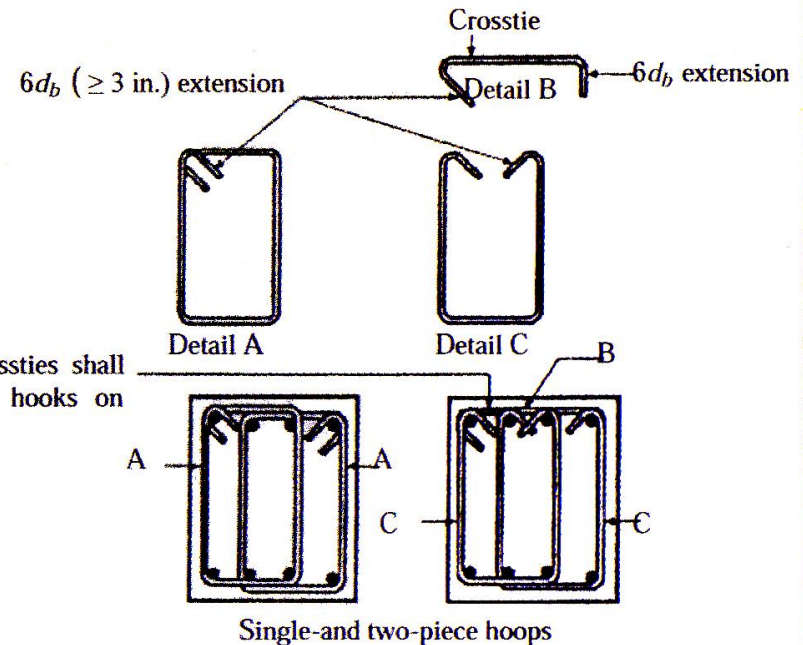


Where hoops are required, lateral support for longitudinal bars per ACI Sec. 7.10.5.3



Section A-A

**Fig. Transverse reinforcement requirements for beams**

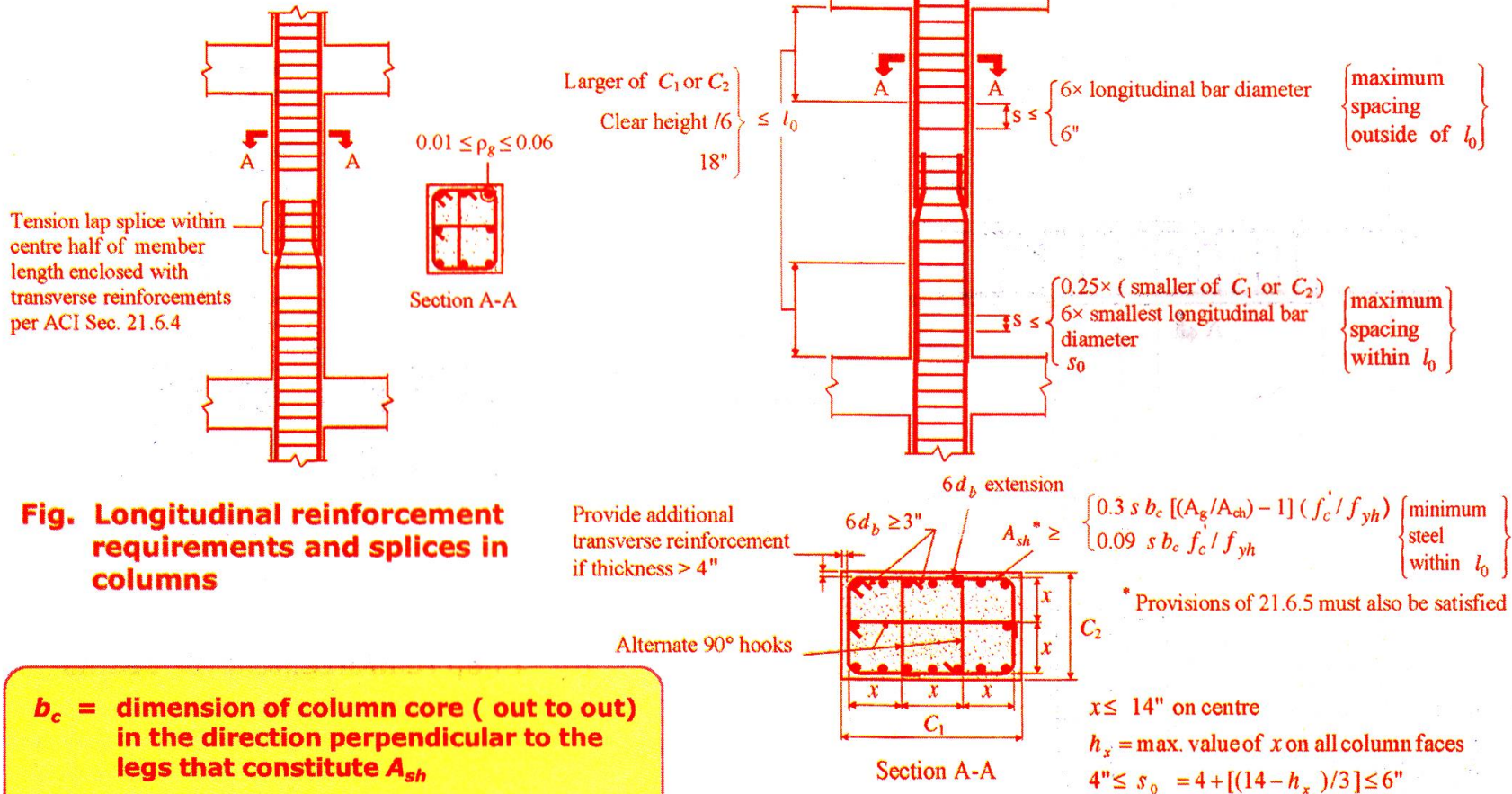


**Fig. Hoop reinforcement for beams**



## (5) Special Moment-Resisting Frame Detailing *contd.*

### Columns



$b_c$  = dimension of column core (out to out) in the direction perpendicular to the legs that constitute  $A_{sh}$

$A_{ch}$  = cross sectional area of column core, measured out to out of stirrup steel

**Fig. Transverse reinforcement requirements for columns (rectangular hoops)**

# Code Provisions and Best Practices



- • Follow MNBC, ACI, Eurocode standards
- • Proper anchorage and lap splices
- • Shear detailing and confinement
- • Detailing improves ductility and resilience
- • Proper management for Captive Effect

Document No. IITGN-WB-EQ4-V3.0

IITGN-WB-EQ5-V3.0

Final Report: IS 13920 Code and Commentary  
IITGN • World Bank Project on Seismic Codes



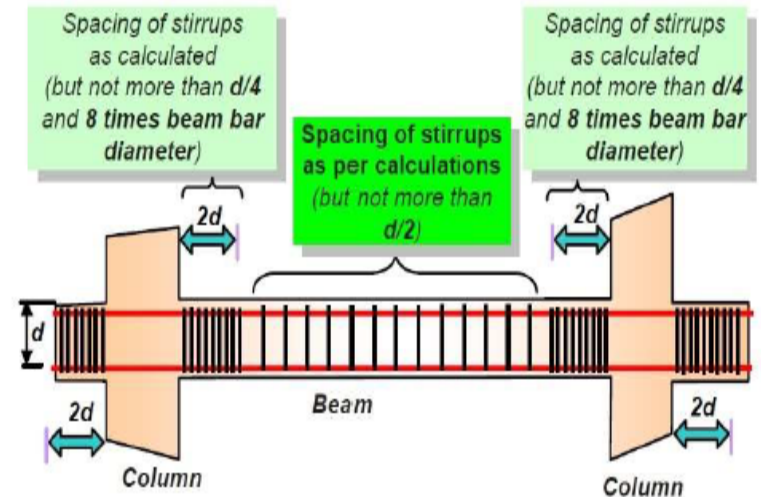
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# **Ductile Design and Detailing of Reinforced Concrete Structures Subjected to Seismic Forces – Code of Practice (IS 13920 : 2016) Proposed Modifications and Commentary**



# Comparative clauses of detailing a beam (Ordinary and Ductile)

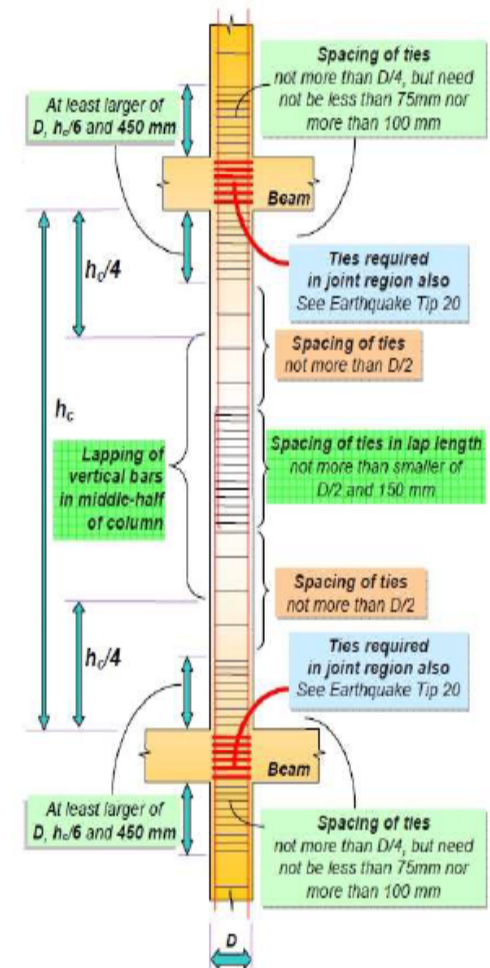
Beam detailing (Ordinary and Ductile)				
Aspect Description	Ordinary detailing (IS 456:2000)		Ductile detailing (IS 13920:2016)	
	Clause	Detail	Clause	Detail
Response reduction factor (as per IS 1893:2016)		$R = 3$		$R = 5$
Axial stress limit	43.2	$\leq 0.2f_{ck}$	6.1	$\leq 0.08f_{ck}$
Width - Depth ratio	--	Not available	6.1.1	$\leq 0.3$
Minimum Width	--	Not available	6.1.2	200 mm
Minimum Depth	--	Design of deep beams are allowed	6.1.3	25 % of Clear span (design of deep beams not allowed)
Flexural reinforcement (Min.)	26.5.1.1 (a)	$85/f_y$ (in%)	6.2.1	$0.24 * (f_{ck})^{0.3} / f_y$ (in%)
Flexural reinforcement (Max.)	26.5.1.1 (b)	4.00%	6.2.2	2.50%
Flexural reinforcement (overriding clauses)	--	Not available	6.2.3 and 6.2.4	Yes, Available
Bond (Anchorage)	26.2.1	Development length only	6.2.5	Development length + (10 Times Bar dia.)
Lap splices (location)	26.2.5	Splices shall be provided as far as from the sections of maximum stress and be staggered	6.2.6.1	Shall not be provided with in joint
				Within distance of 2d from face of the column
				Within quarter length of beam adjoining plastic hinge
	26.2.5.1	When bars are spliced at maximum stressed points such as increasing lap and closer spacing of stirrups		
Transverse reinforcement (Min. Link dia and spacing)	--	No clause specifying min. diameter	6.3.2	Min. diameter of link is 8 mm
	26.5.1.6	Min. shear reinforcement $\geq (0.4*b)/(0.87*F_y)$	6.3.5 (a)	Min. Link spacing $\leq d/4$
	26.5.1.5	Max. Spacing shall be restricted 0.75*d and 300 mm.	6.3.5 (b)	8 times diameter of the smallest longitudinal bar
			6.3.5 (c)	100mm
Transverse reinforcement (closer spacing)	26.2.5.1	Closer spacing of stirrups shall be provided over lap splices	6.3.5.2	Closely spacing over a length 2d on either side of plastic hinge location



### Column detailing (Ordinary and Ductile)

Aspect Description	Ordinary detailing (IS 456:2000)		Ductile detailing (IS 13920:2016)	
	Clause	Detail	Clause	Detail
Response reduction factor (as per IS 1893:2016)		$R = 3$		$R = 5$
Axial stress limit	43.2	$\geq 0.2f_{ck}$	7.1	$> 0.08F_{ck}$
Aspect ratio	--	No specific clauses	7.1.2	(Min./Max.) Dimension $\geq 0.45$
Minimum Dimensions	--	No specific clauses	7.1.1 (a)	20 times max. diameter of bar in the beam anchoring in to column at joint
	--	No specific clauses	7.1.1 (b)	300mm
Long. reinforcement (Min.)	26.5.3.1	0.80%	--	No specific clauses
Long. reinforcement (Max.)	26.5.3.1	6% (But limited to 4%)	--	No specific clauses
Lap splices (location)	SP-34, Fig 7.9A - 7.9 E and IS 456:2000, cl.26.2.5	Lap splice shall be provided at 75mm above floor level. But shall not be provided in the locations where stress can be maximum	7.3.2.1 ©	Shall be provided only in central zone
				Shall not be provided in joint
				Shall not be provided within a distance of 2d from the face of beam
Transverse reinforcement (Min. Link dia and spacing)	26.5.3.2 (c,2)	Diameter shall not be less than $1/4^{\text{th}}$ of largest longitudinal bar dia.	7.4.2 (a)	Min dia. Is 8mm/10mm depending on diameter of main bar
		Spacing shall not be less than the following:	7.4.2 (b, d)	Max. spacing shall be limited to 300mm or half of the least lateral dimension of column
	26.5.3.2 (c,2)	Least lateral dimension of compression members	8.1 (b) (1)	Min spacing shall be less than $1/4^{\text{th}}$ of min. dimension of the column
		16 times the smallest dia of long. Bar	8.1 (b) (2)	Min. spacing shall be less than 6 times the diameter of smallest main bar
		300mm	8.1 (b) (3)	Min spacing shall be 100mm
Cross tie limit		Yes. To be provided when exceeds 300mm	7.4.2 ©	Yes. To be provided when exceeds 300mm
Transverse reinforcement (closer spacing)	--	No specific clauses	8.1 (a)	Shall be provided in locations of flexural yielding only and over lap splices

## Comparative clauses of detailing a column (Ordinary and Ductile)

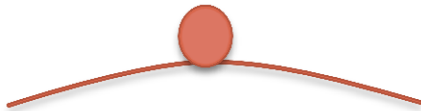


## STEEL STRUCTURE ( AISC Seismic Provisions )

### Structural Stability



Stable Equilibrium



Instable Equilibrium

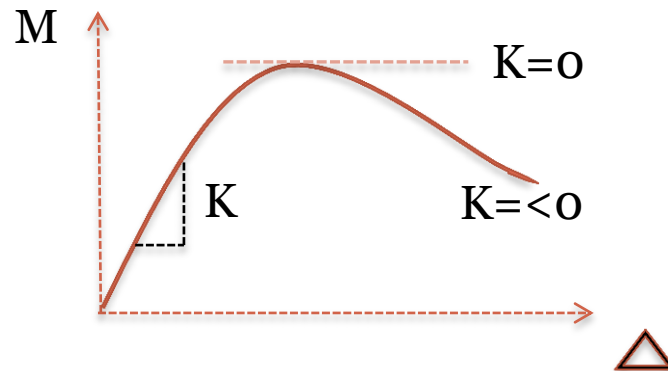


Neutral Equilibrium

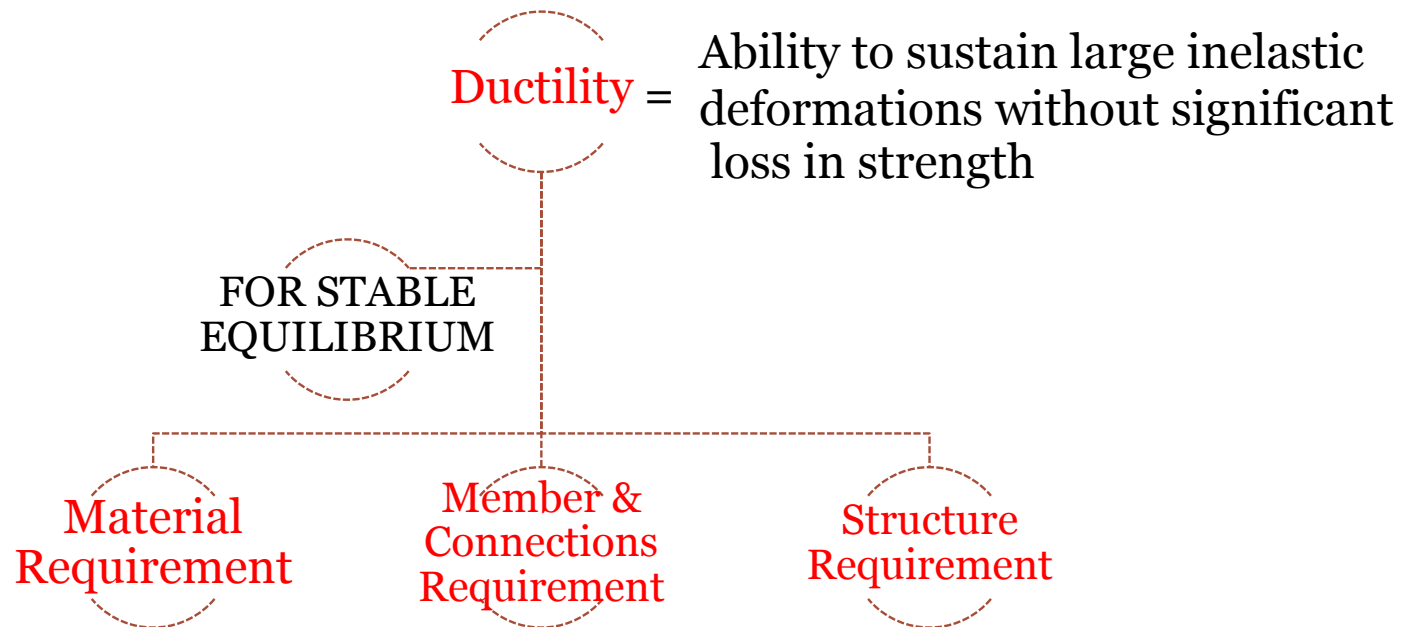
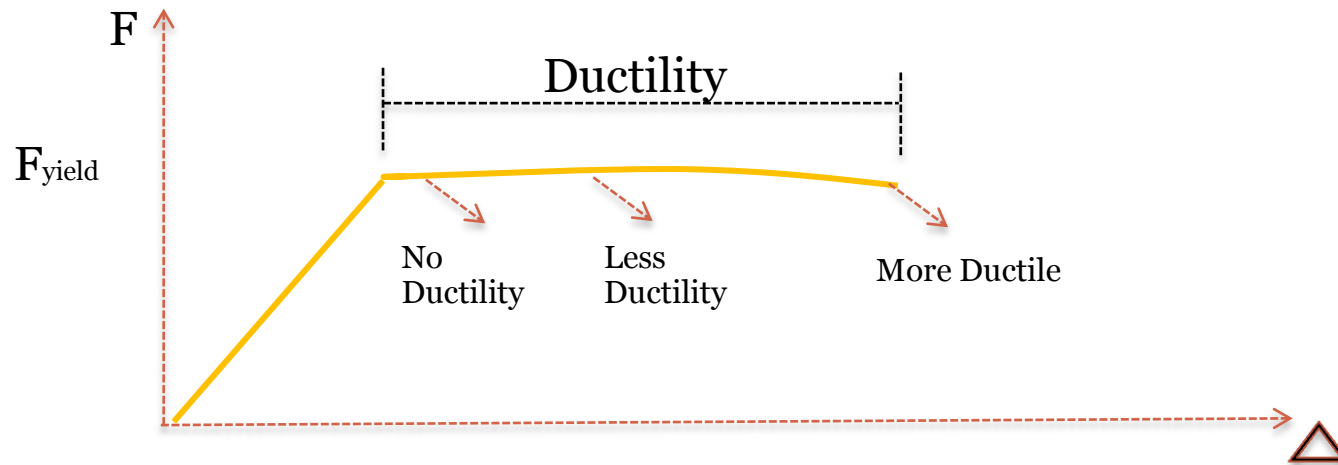
- Structure Stiffness down as Loads up
- Change in stiffness due to large deformation and/or material inelastic
- Load capacity reach when stiffness = 0 ( Neutral Equilibrium )
- When stiffness negative = -ve ( Instable Equilibrium )



Structural Stability Failure







## *Recommended Reference Document*

ANSI/AISC 341-22  
An American National Standard

# Seismic Provisions for Structural Steel Buildings

September 26, 2022

Supersedes the *Seismic Provisions for Structural Steel Buildings*,  
dated July 12, 2016, and all previous versions

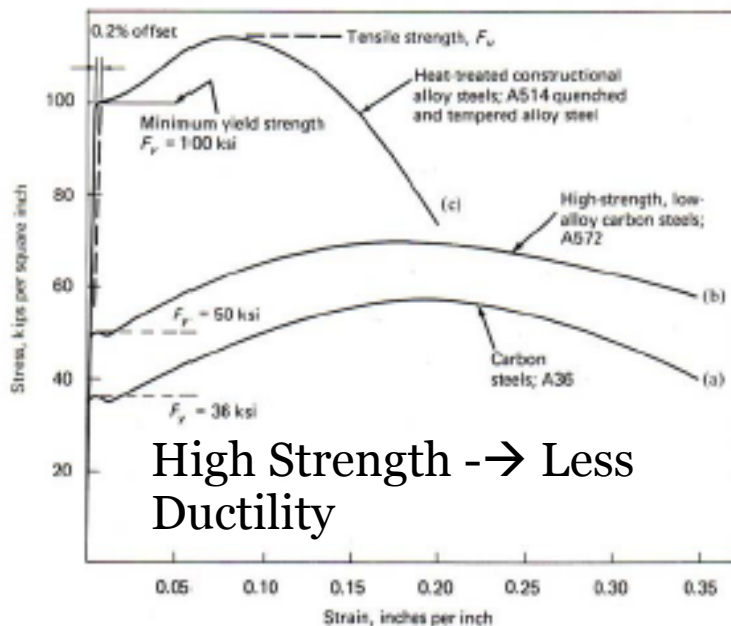
Approved by the Committee on Specifications



**Smarter.  
Stronger.  
Steel.**

# MATERIAL REQUIREMENTS

- Limit maximum Yield Stress = 50 Ksi
- Use expected yield stress  $F_y$  (expected ) =  $R_y F_y$  (min. yield stress )



## TRUE STRENGTH FACTOR

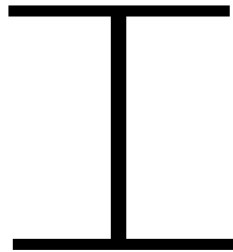
ตารางที่ 2 ค่าตัวคูณเพื่อหาค่าลดราคจริงของวัสดุ[2]

ชนิดของก๊อการลดวัสดุ	$R_y$
เหล็กรีดร้อน (Hot-Rolled Section)	
ASTM A36	1.5
ASTM A572	1.3
เหล็กกลาาง (Hollow Steel Section)	
ASTM A500	1.3
ท่อเหล็ก (Structural Steel Pipe)	
ASTM A53	1.4

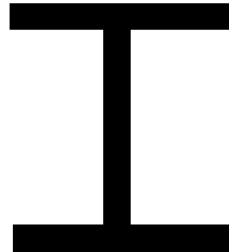


# MEMBER REQUIREMENTS

- Use compact section
- Use expected yield stress  $F_y$  (expected) =  $R_y F_y$  (min. yield stress)
- Use low b/t ratios with adequate lateral bracing

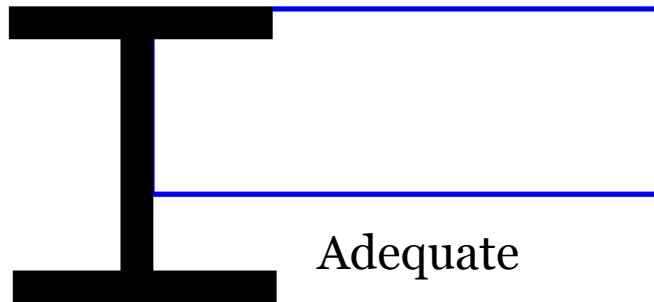


Non-compact  
section

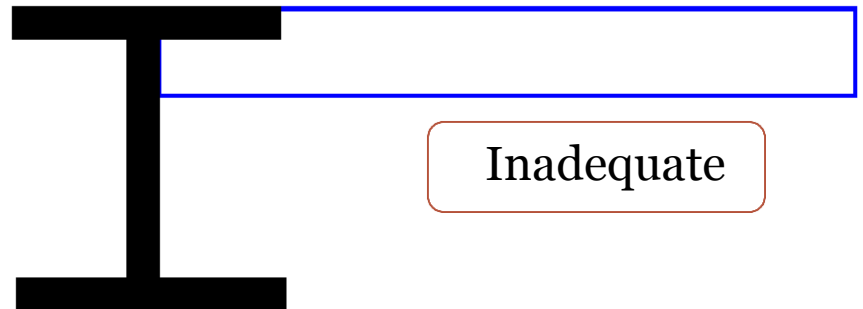


Compact section

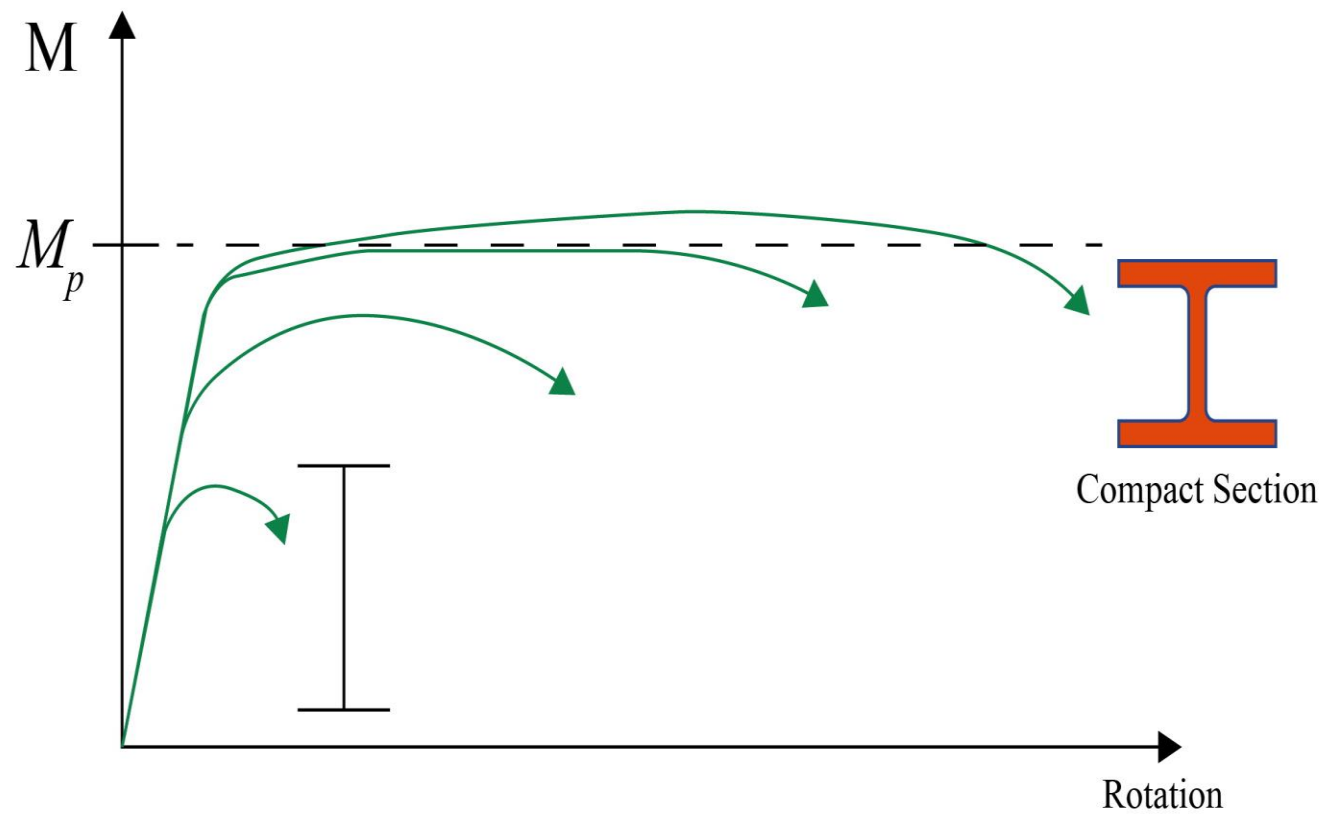
**\* Prevent Lateral Torsional Buckling**



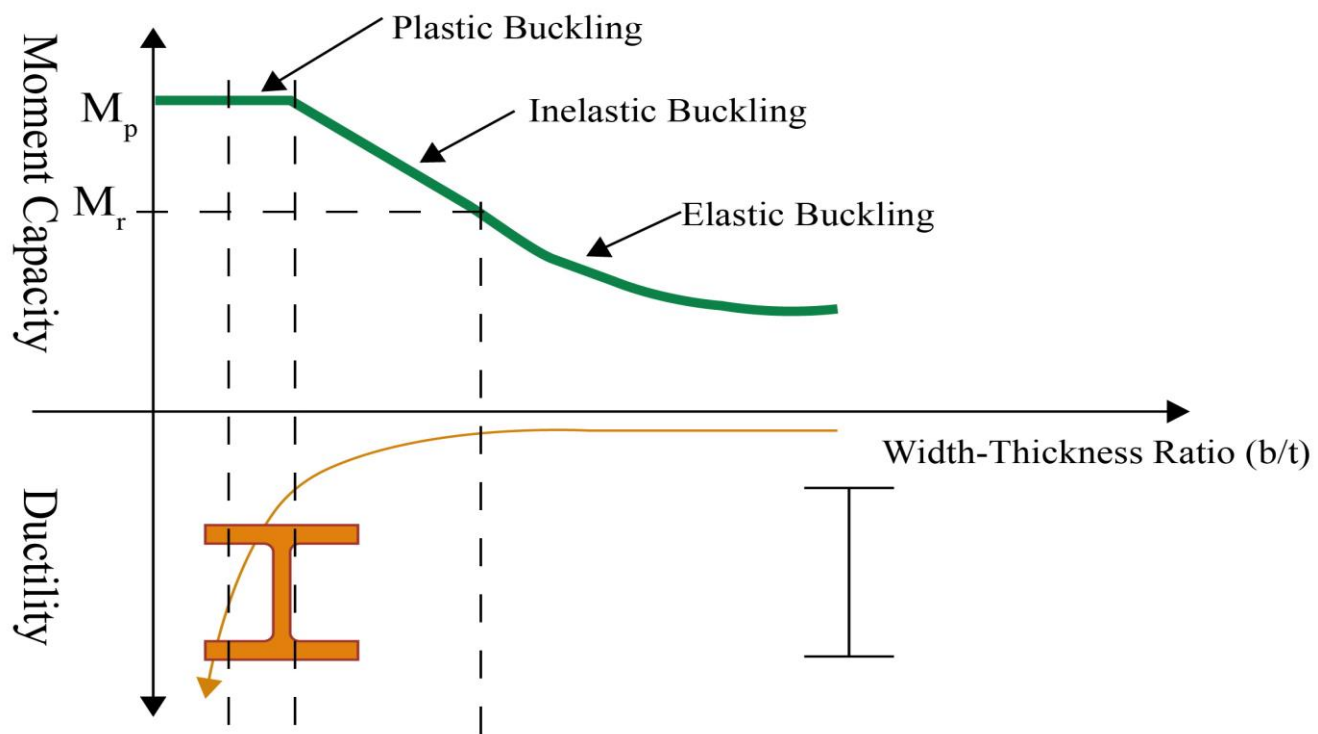
Adequate



Inadequate







# STRUCTURE REQUIREMENTS

## Moment Frame

- OMRF ( Joint design for  $1.1 R_y M_p$  )

### Ductility class medium

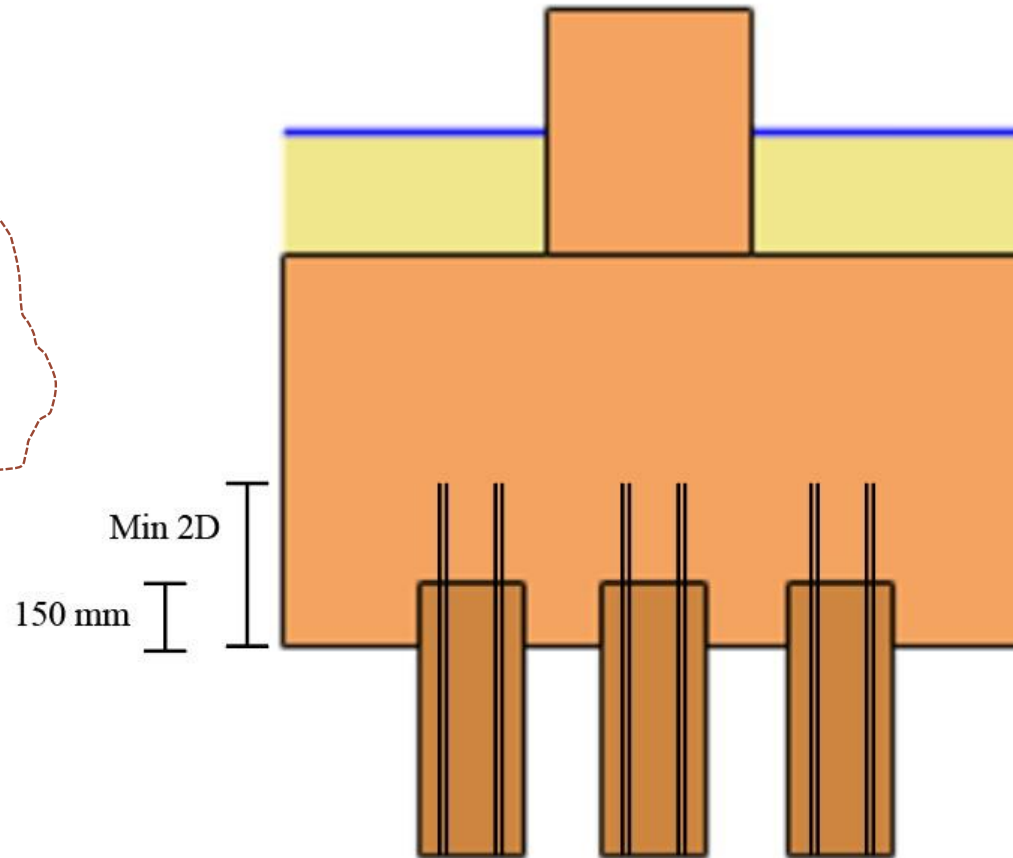
- IMRF ( 0.02 radian rotation requirement at joint )

### Ductility class high

- SMRF ( 0.04 radian rotation requirement at joint )

## Pile Reinforcement Recommendation For Driven Pile / Pressed Pile

**PILE HEAD  
TREATMENT  
IS  
NECESSARY**

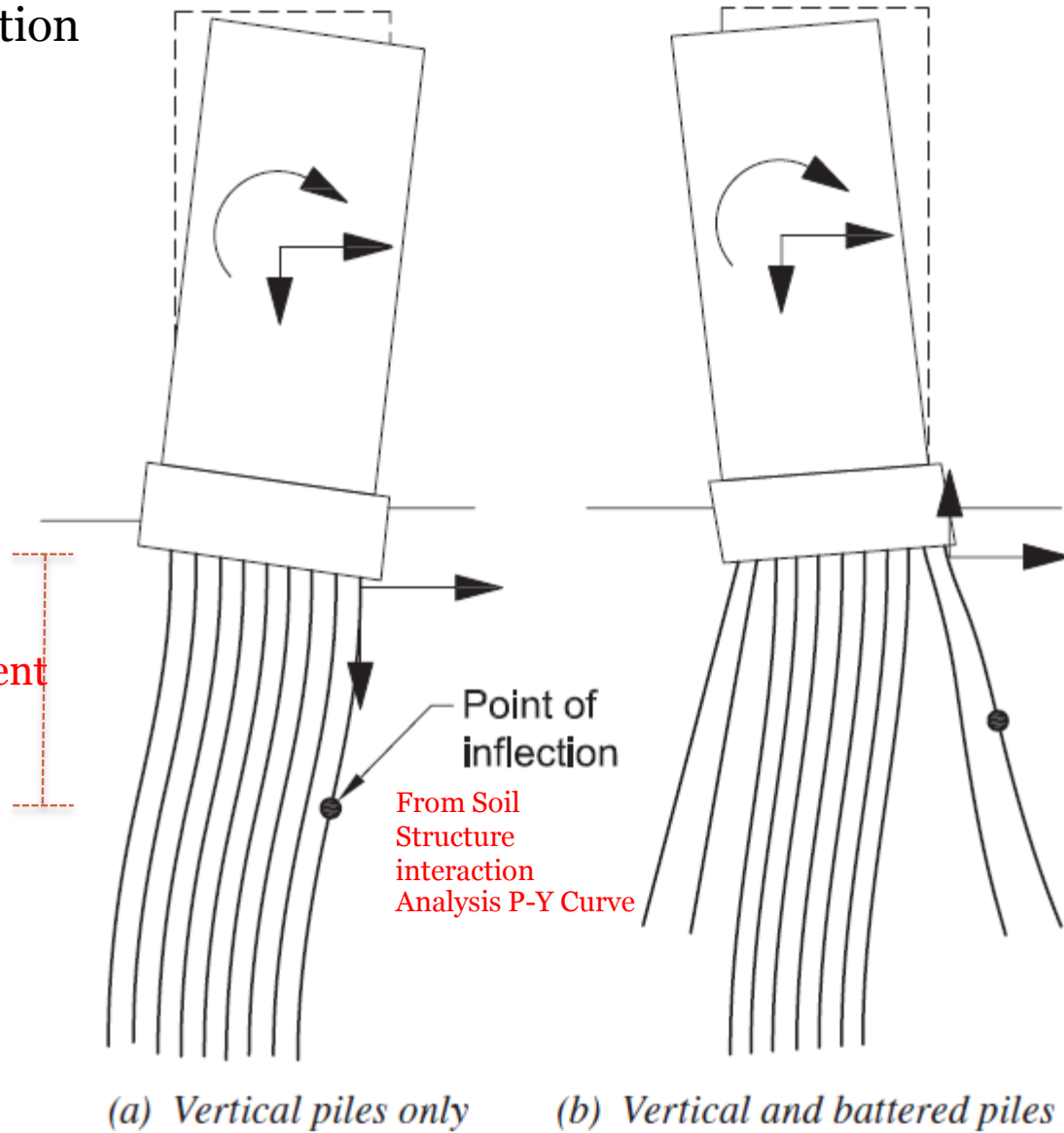


Fixed connection for Ductility & Energy Dissipation



# Pile Reinforcement Recommendation for Bored Pile

Transverse reinforcement spacing =  $\leq 100 \text{ mm}$



C-D4.1. Deformations of piles and forces acting on an individual pile.

# Code Provisions and Best Practices



- • Follow AISC strength limit
  - • Ductile member shall be weakest in the Load Path
  - • Provide connections stronger than members
  - • Avoid high strength steel in ductile elements
  - • Use cross section with low  $b/t$  ratios
  - • Provide adequate bracing
-

# Lessons from Mandalay



- • Importance of code compliance
- • Need for skilled professionals
- • Retrofitting and maintenance
- • Risks of informal construction



# Comparison of Structures



- Properly detailed structures: Minor damage / No damage
- Poorly detailed structures: Severe damage or collapse

Detailing improves performance significantly

# Recommendations



- • Enforce seismic design codes
- • Train foreman, engineers, architects, and workers
- • Retrofit vulnerable structures
- • Conduct public awareness campaigns
  - ✦ Lack of Permit / Inspection
  - ✦ Hiring unskilled/ uncertified workers
  - ✦ Using substandard materials
  - ✦ Inadequate foundation system
  - ✦ Unpermitted extensions ( overloading the original structure )
  - ✦ Lack of material testing
  - ✦ Absence of engineering design, etc.

Poverty & Affordability / Lack of access to formal service /difficult permitting process /  
Traditional construction methods / Lack of awareness for long term risks

# Conclusion



- Earthquake detailing is critical for safety
- Mandalay earthquake highlights the need

Structural safety = Ductile design + Detailing +  
Supervision + Enforcement



For cross border engineering services among Asean countries



## ASEAN OCCUPATIONAL SKILL STANDARD FOR CONSTRUCTION



## LOCAL PRACTICES AWARENESS TRAINING ON CONSTRUCTION COMPLIANCE

For  
Foreign Workers & Foremen

# Importance of Earthquake-Related Detailing in Construction:



Thank you very much  
for  
kind attention

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Any Questions?